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# International Journal for Research in Applied Science & Engineering Technology (IJRASET) Design, Modification and Analysis of Shaft of Concrete Mixer Machine

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Abstract-In this project Design, Modification and Analysis of shaft of concrete mixer machine has done. Shaft is an important equipment of concrete mixer machine use for concrete mixture preparation and for support a revolving drum. The main objective of this analysis is to optimize the design of concrete mixer machine. The existing shaft of concrete mixer machine gets failed after approximately 150 Hr of uses.

To analyse this shaft using FEM, firstly a proper CAD model is developed using Pro/E cad software. Then by using ANSYs software FEM analysis is done to determine the different types of stresses and deflection developed. After carried out the analysis it has been found out that the existing design of shaft of concrete mixer machine is not proper and therefor I had suggested to change the material of the shaft for efficient working and to withstand the different static and dynamic load. Key words: shaft design, computer aided design, mixer.

### I. INTRODUCTION

A concrete mixer machine is also commonly called a cement mixer, is a device that homogeneously combines cement, aggregate such as sand or gravel, and water to form concrete.

Different styles of stationary mixers have been developed each with its own inherent strengths targeting different parts of the concrete production market. A typical concrete mixer uses a revolving drum to mix the components. Today's market increasingly requires consistent homogeneity and short mixing times for the industrial production of ready-mix concrete, and more so for precast concrete. This has resulted in refinement of mixing technologies for concrete production.

To supply continuously the ready mix its necessary that the concrete mixer should be in good condition of working, but it has been observed that the shaft of mixer get failed after some uses of time.

To determine a reasonable structure and technical parameter of continuous mixers is an urgent task. So in this project I am trying to identify the different causes of shaft failure.

It was found that spun pipe manufacturing industry or industry related to manufacturing of cement or concrete product only concentrated on the geometrical properties of reinforced concrete. The geometric property of reinforced concrete is depends upon the proper ratio of input materials and also proper functioning of mixer machine.

It is observed that the shaft of mixer machine bends or it get fractured due to overloading of input mixer. This results into low quality of concrete mixture.

Mixing is a complicated process that is affected by the type of mixer, the mixing cycle as defined by the duration, the loading method, and the energy of mixing.

For most machine shafts, however, analysis should be relatively straightforward. That's because the failure typically provides strong clues to the type and magnitude of forces on the shaft and the direction they acted in, the failed parts will tell exactly what happened. In this project FEM analyse of concrete mixer shaft has done. Shaft is an important equipment use for concrete mixture preparation. It has been observed that the existing concrete mixer shaft of Wainganga spun pipe industry get failed at after some uses of time. So it is very tedious job for the workers to work with bend or braked shaft it may dangerous to worker and complicated to overcome the failures. Also it consumes lot of time and loss of productivity.

# II. DESIGN AND SPECIFICATION

Mixer has following main components:

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- A. Shaft
- B. Drum
- C. Chassis
- D. Blade
- E. Gear
- F. Pulley, Belt and Motor

As there is the problem with the shaft of concrete mixer shaft. Therefor only the designing of existing shaft is check.

III. SPECIFICATION OF SHAFT

- A. Material of shaft: Mild steel 1030
- B. Length of shaft: 630mm
- C. Pedestal dia: 72mm
- D. Dia of shaft: 44mm
- E. Outer dia of thread: 37mm
- F. Inner dia of thread: 33mm
- G. Chamfer length: 155mm
- H. Bottom grease hole dia: 20mm
- *I.* Grease hole length: 360mm



Fig:1 shaft specification

# IV. SPECIFICATION FOR ASSEMBLY DRAWING

Thickness of drum=3mm Upper rod thickness=16mm Upper dia of drum=500mm Middle dia=900mm Bottom dia=600mm Overall height=1000mmInner distance =970mm Outer distance =1150mm Width=100mm Electric motor 3HP Rpm of hopper or drum=25 Pulley dia=555mm

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Fig2: assembly drawing

# V. FORCE CALCULATION

To calculate the different type of forces acting on shaft of concrete mixer machine, I had developed free body diagram of concrete mixer machine.



Figure:3 F.B.D. of concrete mixer machine

# A. Calculation of Force of Impact

As the mixture impacts on front end of shaft, thus I calculated the impact force acted on shaft due to the mixture. But it is observed that only 30% of total mixture is impacted on front end of shaft with reference to company owner and information available on websites. Thus, calculating impact force for 30% of mixture.

```
Mixture proportions:
Cement - 140kg
Sand
           - 80kg
Water
           - 30kg
Aggregates - 50kg
Thus, Total mixture mass is 300kg
Thus calculating impact force for 90 kg of mass that is for 90*9.81= 882.9N
(W/Ymax) = 384EI/5L^{3}
(W/Ymax) = K
            I=∏/64*44<sup>4</sup>
          =183.58*103
          = 384*204*103*183.93*103/5*6203
          = 12.09*10<sup>3</sup> N/mm
Impact force = (2*K*W*H)\frac{1}{2}
           =(2*12.09*10^{3}*882.9*300)^{1/2}
            = 80.03 KN
```

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B. For UDL Weight Calculation

- On shaft of concrete mixer different types of loads are acting
- 1) Because of drum self-weight
- 2) Because of mixture weight
- a) Drum self-weight

F1=m\*g

=30\*9.81

=294.3 N

b) Mixture weight

F2 = m\*g=300\*9.81

=2943 N

c) Drum mean dia.

= 500+900+600/3

= 666.67 mm

d) UDL weight =F1+F2/Mean dia of drum

= 294.3+2943/ 666.67

= 4.86 N/mm

e) Rate of UDL acted on circumference of shaft per mm = shaft dia. \* UDL weight

=44\*4.86

= 0.241 KN/mm

#### VI. TORQUE ON SHAFT EXERTED BY ELECTRIC MOTOR

T=60P/2∏N

=60\*2238/2 ∏\*25 =854.85 N-m =854.85\*10<sup>3</sup> N-mm

A. Stresses in shaft

1) Shear stress due to transmission of torque  $T=16*T/\prod d^3$ =16\*854.85\*10<sup>3</sup>/ $\prod$ \*44<sup>3</sup> =51.109 N/mm<sup>2</sup>

B. For bending stress calculation



Figure 4: load diagram of shaf

# C. By slope deflection method

 Fixed end moment Span BC M'BC= -WL<sup>2</sup>/12 = -0.214\*370<sup>2</sup>/12

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```
= -2.44*10^{3} KN/mm
    M'CB= WL<sup>2</sup>/12
          =0.214*3702/12
           =2.44*103 KN/mm
    Span CD
        M'CD= -Wab2/l2
                = -(0.49*150*70^2/220^2)
                = -7.44 KN-mm
         M'DC = Wa^2b/l^2
                = (0.49 \times 150^2 \times 70/220^2)
                = 15.94 KN-mm
2) Slope deflection equations
        a) MBC= 2EI/L (2\theta B + \theta C)+M'BC
            =2EI/370 (2\theta B + \Theta c) - 2.44 \times 10^3 \dots 1
        b) MCB= 2EI/L (\Thetab+ 2\thetac)+M'CB
             = 2EI/370 (\Theta b + 2\theta c) + 2.44 * 10^3 \dots 2
        c) MCD= 2EI/L(2\theta C+\theta D)+M'CD....(\Theta d=0)
              =2EI/220 (2θC) -7.44 .....3
        d) MDC= 2EI/L (\thetaC)+M'DC
               = 2EI/220 (\theta C) + 15.94 \dots 4
3) Equilibrium equation
     At 'B'
    MBA = -Wl^2/2-Wl
         = -0.214 \times 30^{2}/2 - 80.03 \times 30^{2}
         = -2.497*10<sup>3</sup> KN-mm
    MBA+MBC=0
    -2.497*103+2EI/370 (20B+0C)-2.44*103=0
    4EI0B/370+2EI0C/370=4.94*10<sup>3</sup>.....(A)
    At 'C'
    MCB+MCD=0
    2EI/370 (0B+20C)+2.44*103+2EI/220(20C) -7.44=0
    2EI\theta B/370 + 4EI\theta C/370 + 4EI\theta C/220 = -2.43*10^{3}
    2EI0B/370+2360/81400 EI0C = -2.43*10<sup>3</sup>.....(B)
    By solving equation (A) and (B)
    We get,
    \theta B = 550141.59/EI \text{ rad}
    θC= -186383.18/EI rad
4) Final fixed end moments
MBA = -2.497*10<sup>3</sup> KN-mm
MBC = 2.5*10^3 \text{ KN-mm}
MCB= 3.398*103 KN-mm
MCD= -3.396*103 KN-mm
MDC = -1.678*10<sup>3</sup> KN-mm
    MAXIMUM MOMENT= 3.398*103 KN-mm
```

 $\mathbf{W} = \mathbf{W} + \mathbf{W} +$ 

5) Reactions on shaft

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Span ABC:  $\in$  McF=0 -80.03\*400-0.24\*400<sup>2</sup>/2\*+RB\*370-2.5\*10<sup>3</sup>+3.39\*10<sup>3</sup>=0 RB= 130.38KN Span CD:  $\in$  McF=0 3.39\*10<sup>3</sup>+0.49\*150+1.678\*10<sup>3</sup>-RD\*220=0 RD= 23.73KN  $\in$ Fy=0 RB+RC+RD= 80.03+0.214\*400+0.29+0.49 130.38 +RC+23.37 = 166.41 RC= 12.66 KN



Figure 5: S.F.D. and B.M.D.

```
D. Shaft subjected to bending moment
     M/I = \sigma b/Y
     Where;
     M = Bending moment
     I = Moment of inertia & cross-section area of shaft
     \delta = Bending stress
     Y = Distance from neutral axis to outer most shaft
     I = \prod / 64 * d^4
            Y=d/2
     M=3.398*103 KN-mm
     I = \prod / 64 * 44^4
      =183.58*103
     Y=22
     \sigma b = 406.33 \text{ N/mm}^2
E. Maximum shear stress
     T max= 16/\pi d^{3*}(M^2+Td^2)^{1/2}
            = 16/\pi 44^{3*}((3.398^{*}10^{6})^{2} + (854.85^{*}10^{3})^{2})^{1/2}
     T max = 209.49 N/mm^2
```

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= 296/2 = 148 N/mm<sup>2</sup>

T allowable (148MPa) < Tmax (209.49 MPa) Hence, shaft get failed.

F. Von mises stress (according to distortion energy theory)

 $\sigma eq = (\sigma b^2 + 3\tau^2)^{1/2}$   $= (406.33^2 + 3*51.109^2)^{1/2}$   $= 894.05 \text{N/mm}^2$   $\sigma eq \text{ allowable= ultimate tensile strength/ safety factor}$  = 527/2  $= 263.5 \text{ N/mm}^2$   $\sigma eq \text{ allowable (263.5 MPa)} < \sigma eq (894.05 MPa.$ Thus, shaft get failed.

#### VII. FATIGUE ANALYSIS OF SHAFT BY ANALYTICAL APPROACH

Fatigue analysis is carried out to found out the endurance strength of shaft and factor of safety of shaft. We know, Max bending moment and min bending moment are: (Mb)max =3.398\*10^6 N-mm (Mb)min =2.5\*10^6 N-mm To find mean and alternating stress; (Mb) mean =1/2 (Mb)max+(Mb)min =1/2 3.398\*10^6+2.5\*10^6 =2.95\*10^6 N-mm (Mb)alt = 1/2 (Mb)max-(Mb)min = 1/2 3.398\*10^6-2.5\*10^6 = 0.45\*10^6 N-mm Thus, mean and alternating bending stress are: ( $\sigma$ x)mean=32(Mb)m/ $\pi$ d<sup>3</sup>

 $=32*2.95*10^{6}/\pi(44)^{3}$ 

 $(\sigma x)$ alt =32(Mb)a/ $\pi$ d<sup>3</sup>

```
=32*0.45*10^{6}/\pi(44)^{3}
```

= 53.81 N/mm<sup>2</sup>

```
We have, Max torque:
```

```
Tmax= 854.85*10<sup>3</sup> N-mm
```

For Tmin I measured a current required to rotatea empty mixer :

```
Power = current * voltage *\cos\emptyset
```

```
= 5 \text{amp}*440 \text{v}*0.8
```

= 1760w

Tmin = 672.27\*10<sup>3</sup> N-mm

```
Thus, mean and alternating torque are:
```

Tmean =  $\frac{1}{2}$ \*(Tmax+Tmin)

= 763.56\*10<sup>3</sup> N-mm

Talt =  $\frac{1}{2}$ \*(Tmax-Tmin)

= 91.29 N-mm

Thus, mean and alternating shear stress are:

T mean=  $16*Tm/\prod d^3$ 

 $= 16*763.56*10^{3} / \prod *44^{3}$ 

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= 45.62 N/mm<sup>2</sup>  $Talt = 16*Ta/ \prod d^3$ = 16\*91.29\*10<sup>3</sup>/ []\*44<sup>3</sup> = 5.45 N/mm<sup>2</sup> A. Fatigue stress concentration factor for bending Kf = (K-1)\*q+1= (2.28-1)\*0.22+1= 1.282 B. Fatigue stress concentration factor for torsion Kfs = (Ks-1)\*q+1=(1.82-1)\*0.22+1= 1.180Where, K= stress concentration factor for bending Ks=stress concentration factor for torsion q =Notch sensitivity factor For D/d=1.6 & r/d= 0.045 C. Thus, equivalent or von mises stresses calculation  $\sigma m = ((\sigma x m * kf)^{2} + 3(\tau m * kfs)^{2})^{1/2}$  $=((352.75*1.282)^2+3*(45.65*1.180)^2)^{1/2}$ = 461.75 N/mm<sup>2</sup>  $\sigma a = ((\sigma xa * kf)^{2} + 3(\tau a * kfs)^{2})^{1/2}$  $=((53.81*1.282)^2+3*(5.45*1.180)^2)^{1/2}$ = 69.88 N/mm<sup>2</sup> Stress at mean condition is max thus, consider  $\sigma$ m= $\sigma$ eqi= 461.75 N/mm<sup>2</sup>  $Tan\theta = \sigma a/\sigma m \& also Tan\theta = Sa/Sm$ = 0.80 .....(A) D. Endurance strength To find endurance strength 'Se' Se= A\*K size\*K surface finish\*K temp\*K reliability\*se'/kf But se'= 0.5 \* sut= 0.5\*527 $= 263.5 \text{ N/mm}^2$ A=1(for bending) A=load factor Ksize= 1-(d-12.5/75-12.5\*1-Kz')-----(Kz'=0.84 for M.S.) = 0.92Ksurf = 0.92 (for ground finish) Kreli = 90% = 0.897

Assume Ktemp= 1

Se= 127.22 N/mm<sup>2</sup>

Kf = 1.282

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E. Goodman's equation Sa/Se + Sm/Syt=1 0.8\*Sm/127.22 + Sm/296=1By solving we get, Sm=103.45N/mm<sup>2</sup> Sa=82.76 N/mm<sup>2</sup> Where; Sa = amp. Normal stress Sm = mean normal stress Sm = mean normal stress Syt = yield tensile strength F.O.S= Sa/ $\sigma$ a = 82.76/69.88 = 1.18

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#### VIII. FINITE ELEMENT METHOD

Finite Element Method is the micro mechanical analysis which is now days used as a powerful and an efficient tool for understanding the stress strain behavior of the structure. The basic idea in the Finite Element Method is to find the solution of complicated problem replacing it by the number of smaller regions. Thus, the solution of each region is considered as built up of many small interconnected sub regions called Finite Elements.



Figure6.3D model of shaft

A. Moment applied on the shaft

Figure shows the moment which is applied on the shaft.



Fig:7. Moment applied on shaft

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B. Force applied on the shaft

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Fig:8. Force applied on the shaft

C. Equivalent stress results



Figure 9 Equivalent stress

Equivalent stress of shaft is 315.31MPa which is greater than allowable stress of 263.5 MPa.

D. Maximum shear stress results



Figure 10 Maximum shear stress

Max. shear stress of shaft is 182.5 MPa which is greater than allowable stress of 148 MPa

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E. Life cycle results



Figure 11life cycle of shaft

# F. Safety factor results



Figure 12.Safety cycle

Safety factor of shaft is 0.856 which is less than 1. Thus, design is failure. SOLUTION 1:

Table 1 Comparison of Allowable stresses and Ansys result:

		5
		ALLOWABLE STRESSES
STRESSES	ANSYS RESULTS	
Equivalent stress	315.31 MPa	263.5 MPa
Max. shear stress	182.05 MPa	148 MPa
	F.O.S=0.856	F.O.S>= 1

<sup>1)</sup> It has been observed from above table 22 which is obtained by FEM analysis of shaft of concrete mixer machine that maximum shear stress and equivalent stress both are greater than allowable shear and equivalent stresses of existing shaft material

2) Thus, failure occurs in the shaft of concrete mixer machine.

- 3) Thus, its need to change the parameter of shaft it may be either dimensions or by changing the material of shaft.
- 4) Due to the design limitations set by manufacturer of concrete mixer machine, I made a modification of shaft by changing the material of shaft.

# IX. MODIFIED DESIGN

Redesign of shaft by using different material:

•SAE 4140 (Chromium Molybdenum Steel)

•SAE 4140 alloy Steel is chromium, molybdenum alloy steel. It has high fatigue strength, abrasion and impact resistance, toughness

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and torsion strength etc. It is used extensively in most industry sectors for a wide range of application such as axle shaft, bolts, crankshaft and part lathe, spindle, motor shaft, nut, pinions, pump shaft, worm, etc.

•Ultimate Strength (Sut) = 815 MPa

- •Yield Strength (Syt) = 680 MPa
- A. Equivalent stress



Figure: 11.Equivalent stress developed on modified shaft

Equivalent stress developed on shaft is 315.06 which is less than Allowable stress of material of modified shaft.

B. Maximum Shear stress



Figure: 12.Maximum Shear stress developed on modified shaft

Maximum shear stress developed on shaft 181.9 is less than Allowable shear stress of material of modified shaft.

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C. Life cycle

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Figure: 13.Life cycle of modified shaft

#### D. Safety Factor:



Figure: 14.Safety Factor of modified shaft

Safety factor of modified shaft is 1.2696 which is greater than 1. Hence it is conclude that modified shaft design is safe.

# X. RESULT AND DISCCUSION

As decided in the objectives all the components of concrete mixer machine were modeled as per specified dimension by using Pro/E software and then assembled.

After that FEM analysis of shaft was carried out with the help of Ansys software and different stress and deformation were calculated. And following solution has been obtained

Tuble2 Comparison of Anowable successes and Ansys result.				
	ANSYS RESULTS	ALLOWABLE		
STRESSES		STRESSES		
Equivalent stress	315.31 MPa	263.5 MPa		
Max. shear stress	182.05 MPa	148 MPa		
	F.O.S=0.856	F.O.S>= 1		

Table2 Comparison of Anowable suesses and Ansys result.		Table2 Con	nparison	of Al	lowable	stresses	and A	Ansys	result:
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It has been observed from above table no. 25 which is obtained by analytical approach and FEM analysis of shaft of concrete mixer machine that maximum shear stress and equivalent stress both are greater than allowable shear and equivalent stresses of existing shaft material. Thus, failure occurs in the shaft of concrete mixer machine.

Therefore, shaft is redesigned by changing material of existing shaft.

After doing the FEM analysis on modified shaft I got the following results;

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Table 3 Comparison of existing shaft and modified shaft and Result from Ansys:

1	U				
SPECIFICATION	SAE 1030		SAE 4140		
Young's modulus MPa	204		206		
Poisons ratio	0.3		0.33		
Density kg/m^3	7800		7700		
RESULT FROM ANSYS					
	Result from	Allowabl	Result from	Allowable stress	
	ansys	e stress	ansys		
Max. shear stress MPa	182.05	148	181.9	340	
Equivalent stress MPa	315.31	263.5	315.06	407.5	
F.O.S	0.856	>1	1.2696	> 1	

Above Table No. 24 indicates that maximum shear stress developed on existing shaft is 182.05 MPa which is greater than a value of allowable shear stress of 148 MPa. Thus, shaft gets failed.

Therefore, shaft is redesigned by changing shaft material to SAE 4140. As Table No.24 indicates allowable shear stress of modified shaft is181.9 MPa which is less than a value of allowable shear stress of modified shaft of 340 MPa. Hence this design is safe.

# XI. CONCLUSION

The structural static analysis of concrete mixer machine shaft is carried out to find out the different failure in the shaft due to different loading condition. By conducting FEM analysis of existing design of the shaft it has observed that maximum shear stress and equivalent stress induced in the shaft is exceeding the allowable shear stress and equivalent stress. Therefore, shaft gets failed. So it is necessary to redesigned shaft.

The property of shaft can be improved either by changing its dimension or by changing material. But due to machine space constant it is not possible to increase the diameter of shaft. Therefore, the shaft is redesigned by taking new material and after conducting again the FEM analysis of shaft with change material. The maximum shear stress and equivalent stress are within limits or less than allowable limits. Therefore, design is safe. Life cycle of shaft and safety factor is also calculated by analytical method and later it is validated by using Ansys software.

# XII. FUTURE SCOPE

- A. In this project design of shaft is analyzed by changing the material.
- B. In future the design of shaft can be analyzed by changing its diameter.
- C. Design of different components of the mixer can also be optimized.
- *D*. In this project, shaft is only analyzed by using static condition, it is possible to analyze shaft by using dynamic condition as the load continuously varying inside the drum.

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