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An Integrated Passive Cooling System for Thermal Comfort

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Abstract: *In the hot and humid environment of Indian summers, a conventional cooling system is too expensive for most people. In this project, Passive cooling systems which consume less power, are more efficient, cost less, and make very little noise are used.*

After researching various passive cooling techniques in isolation and running simultaneously, we aim to develop a system that is cost-effective and efficient at cooling the Indian household.

The focus of this project is on the four major types of passive cooling techniques, they are radiant cooling, solar chimneys, wind catchers, and shading devices.

Supplementary techniques like terrace cooling are also included. The initial analysis and study of the windcatcher system with various heights and inlet shapes have been conducted. A software model has been generated using fusion 360, analyzed in Ansys fluent, and results were recorded.

The radiant cooling system has been designed and an analysis of the system is done. Once the individual system analysis is successful, an integrated model containing all four systems will be generated and analyzed.

The integrated system hence designed will ensure that there is cooling obtained in the room using low-energy passive cooling techniques.

I INTRODUCTION

India is a country with varied climates and a significant portion of the country is living in a hot and humid environment[1]. While many people long for relief from the scorching heat of the sun, an air conditioner is a luxury, that most can't afford. In a developing country like India, the need for affordable cooling is becoming increasingly apparent. The project aims to provide an affordable cooling system that is accessible to a larger population than it was previously available to.

Conventional cooling has some disadvantages that can be improved with this project. It is costly to purchase and install. Requires frequent maintenance for optimal performance. It has many moving parts which lead to multiple points of failure and consume a massive amount of electricity.

These aspects of conventional cooling make it unsuitable for the majority of the population. However, passive cooling is different. Passive cooling systems consume less power, are more efficient, cost less, and make very little noise[2]. They are the ideal system for cooling in the Indian market. This project has the potential to be beneficial not just to any single individual but to the environment too.

It will benefit the common man by being cheaper than a conventional system and consuming less electricity at the same time. Since it consumes less electricity, it also reduces the fossil fuels burned to support the environmental impact of burning fossils. The HVAC industry is one of the largest consumers of electricity[3]. The project has the potential to reduce that consumption by a considerable margin.

The aim of this project is to analyze, design and fabricate a contained passive/hybrid cooling system.

- 1) To compare the statistical difference in performance between different passive cooling devices.
- 2) To evaluate the effectiveness of selected passive cooling devices..
- 3) To determine the rate of cooling in different passive cooling systems due to varied parameters.
- 4) To develop an optimal structure for a radiant cooling system.

II METHODOLOGY

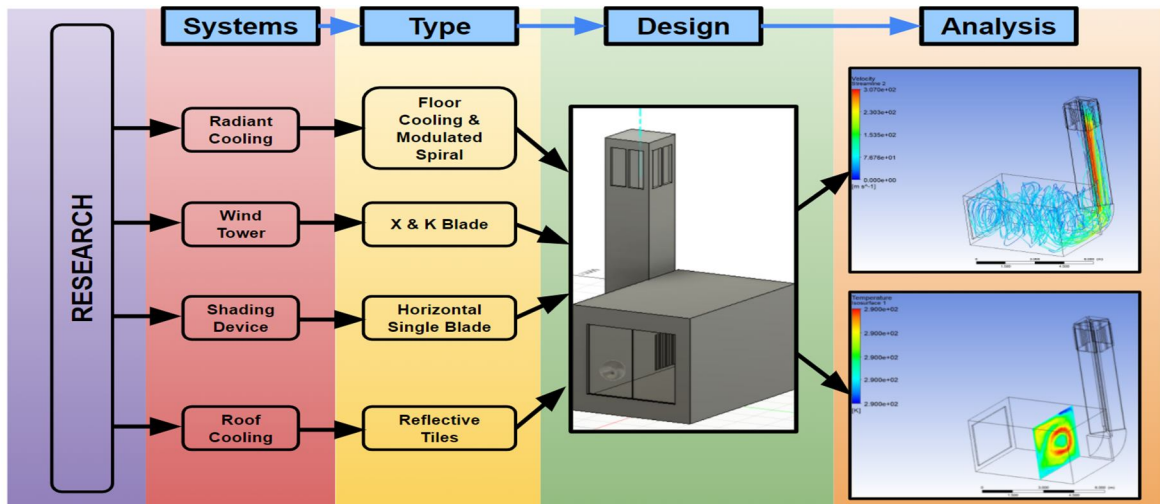


Figure 1: Methodology

In this project, some research papers have been explored. Based on the research papers, the shortcomings and findings of research done on passive and hybrid cooling were analyzed. With the knowledge gained, a prototype will be fabricated based on the design finalized using software like SolidWorks, Ansys, etc. The final product will aim to compensate for some of the shortcomings noticed in previous research. The design will be for a residential apartment.

Simulations will be conducted on the finalized design of the model using Ansys having a fixed set of parameters including orientation w.r.t. to the sun, ambient temperature and humidity, wind flow, and other factors.

III DESIGN

In our design, we decided to incorporate the wind tower and radiant cooling system. A structure that was both performant, included the cooling mechanisms necessary and did not pose unnecessary challenges in the analysis stage was designed.

A. Wind Tower

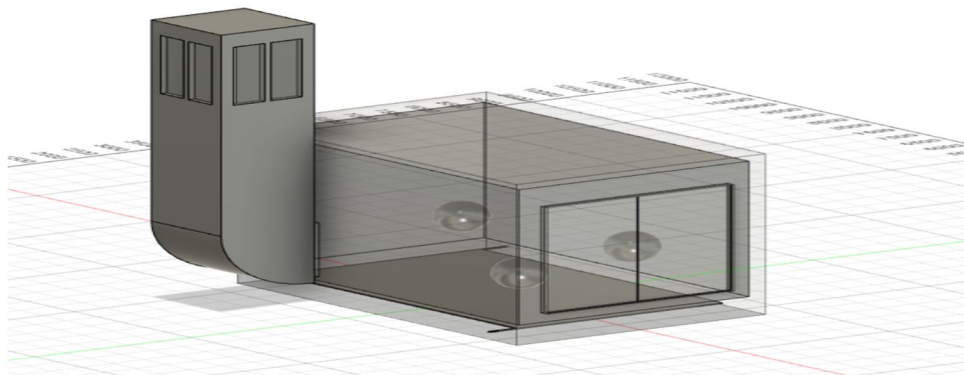


Figure.2 Wind Tunnel Model

*In this finalized structure the dimensions of the room are

Room length: 6000mm (5700mm)

Room breadth: 4000mm (3700mm)

Room height: 4115mm (35000mm)

The properties of the materials used in the analysis are:

Glass properties

Density: 2500 kg/m³

Thermal conductivity: 0.8W/mK

Specific Heat: 0.8 J/g/K

Gypsum properties

Density: 2320 kg/m³

Thermal conductivity: 0.5W/mK

Specific heat: 1138J/g/K

And the dimensions of the wind tower are

Dimension of wind tower inlet: 1500x500mm

Height of the tower from the ground: (from 3m to 9m subject to analysis conditions)

length/breadth (cross-section) of tower: 1500mm

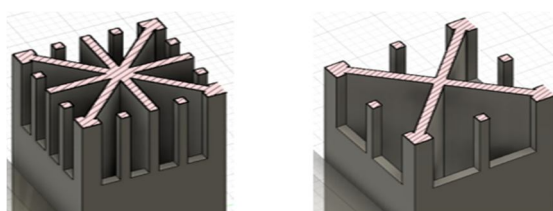


Figure.3 Cross Section of Wind Catcher (a)K-Blade (b)X-Blade

One of the questions the team attempted to solve in the proceeding analysis was if there was a performance difference between the x-blade and k-blade-styled wind catchers in our experiment's climatic conditions, this question arose due to conflicting information obtained in the research phase Hence, the structure of the Wind Tower was designed to accommodate both x blade and k blade windcatchers.

B. Radiant Cooling System

We also chose a radiant cooling system design based on a variety of factors as shown in table 1

TABLE I Factors involved in the design of radiant cooling system[4]

| Parameter | Counterflow | Serpentine | Modulated Spiral | Comment | Inference |
|----------------------------------------------------------------------------------------------------|-------------|-------------------------------------------------------------------------------------------------------------------|------------------|-------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------|
| Impact of the water velocity | ---x--- | Negligible effect | ---x--- | Water velocity has negligible effect | Water velocity= 0.5-1 m/s |
| Impact of the supply water temperature | ---x--- | Similar increasing trend during the heating process when the pipe water temperatures are varied from 35° to 50°C. | ---x--- | The temp rise is faster with a higher temp of the water. However, Avg Temp is reached at about 3hrs in all temperatures | Heating Period can be reduced if a higher water temp is used. A detailed study is required for optimal water temp and heating time for the least energy |
| Average core surface temperature (°C) at Inlet Water Temp = 45°C Inlet Water Velocity = 0.85m/s | 38.026 | 37.727 | 38.418 | | Modulated Spiral has the best avg. temp. although the values don't vary a lot of |

| Homogenization level (Temp at various points on the surface) | Better | Good | Best | | Most Homogeneous Temp distribution in Modulated Spiral |
|--------------------------------------------------------------|--------|------|---------------------|---------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------|
| Pressure losses | Better | Good | Best (Least Losses) | It is clear that for a fixed tubing diameter, an increase of the velocity causes an increase in the pressure losses | Modulated Spiral offers least losses |

Hence, the Modulated Spiral type was chosen.

C. Calculations for a radiant cooling room according to ASHRAE 2019 [5]

A room of 5 occupants in Mumbai, peak temperature 40°C and 86%rh is to be maintained at 24°C and 40%rh Dew point temperature of the room = 9.6°C

Moisture content = 0.0087054kg/m³

- *Step 1:* Determine the sensible and latent hourly heat gain for the room. The sensible and latent hourly heat gains are found using accepted procedures found in the ASHRAE handbooks

In this case let's assume the formula for sensible heat

$$h_s = c_p \rho q dt$$

Where

h_s = sensible heat (kW)

c_p = specific heat of air (1.006 kJ/kg °C)

ρ = density of air (1.202 kg/m³)

q = air volume flow (m³/s)

dt = temperature difference (°C)

Assuming the air flow to be 1,

$$h_s = 1.006 \times 1.202 \times 1 \times 16 = 19.347 \text{ kW}$$

- *Step 2:* Determine the mean water temperature required for cooling

Supply water temperature = 9.6°C (A bit higher than the dew point temperature)

Assuming a temperature rise by 3K, inlet water temperature is 13°C.

- *Step 3.* Determine the minimum air supply required for the room. According to ASHRAE tabulated data. But it is assumed it to be 1m³/s

- *Step 4a.* Determine the latent load capacity of the air:

$$NP * OCPL \times 1.2 \times 2500 \times (HRODA_2 - HRIDA) = \text{___ W}$$

$$5 * 0.05861 * 1.2 * 2500 * (0.86 - 0.4) = \mathbf{404.409 \text{ W}}$$

- *Step 4b:* Determine the sensible cooling capacity of the primary air:

$$V \times 1.2 (DBIDA - DBSUP) = \text{___ W}$$

$$1 * 1.2 * (40 - 24) = \mathbf{19.2 \text{ W}}$$

Where

NP = number of occupants in the space

OCPL = latent heat produced by the occupants

HRODA₂ = humidity ratio of space air

HRIDA = humidity ratio of space operating design condition

V= volumetric flow rate of the supply air

DBIDA = dry bulb temperature of space operating design condition

DBSUP = dry bulb temperature of supply air

- Step 5. Determine the sensible load capacity of the air with the following equation:

$$Q_s = Q_p C_p (t_{room} - t_{supply}) \times 60$$

$$= 1 \times 1.2 \times (24 - 9.6) \times 60 = 1036.8 \text{ kJ/h} = \mathbf{0.288 \text{ kW}}$$

Total sensible cooling required is $0.288 \times 4/3 = \mathbf{0.384 \text{ kW}}$

- Step 6. Select a panel surface temperature at least 2 K higher than the space operating dew-point temperature (13°C) Thus, the required temperature is higher than the MWT calculated in step 2.

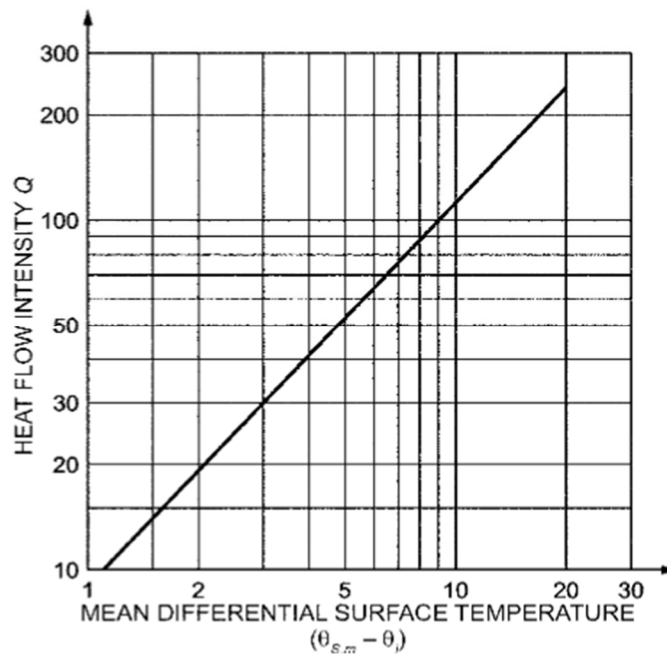


Figure.4 Heat Flow vs Differential surface Temperature [5]

- Step 7. From the 12°C panel operating temperature or panel mean water temperature, derive the supply water temperature and water temperatures to and from the panels. Typically, the difference between supply and return water temperature is 4 K, so the panel water supply temperature, in this case, is 9.6°C and the panel return water temperature is 14.6°C.

- Step 8. Get the output of cooling capacity w.r.t. Temperature.

Heat Exchange Coefficient Between Surface and Space

Floor cooling: $q = 7(\theta_{s,m} - \theta_i) = 7(24 - 15) = \mathbf{49}$

Using an injection circuit requires a circulating pump to provide a constant flow of water through the floor.

Sensible heat load $Q_s = 0.384 \text{ kW} = 1310.366 \text{ btu/hr}$

Inlet Temp. (t_1) = 11°C = 51.8 °C

Outlet Temp. (t_2) = 13°C = 55.4 °C

Therefore, Water Flow Rate $q_1 = Q_s / ((500 \times (t_2 - t_1))) = 1310.366 / ((500 \times (55.4 - 51.8)))$
 $= 0.728 \text{ gpm} = \mathbf{45.93 \text{ cm}^3/\text{s}}$

Volumetric flow rate = $A \times L/t$

$q_1 = (\pi/4 \times d^2) \times v$

$45.93 = (\pi/4 \times 2.34^2) \times v$

$v = \mathbf{10.68 \text{ cm/s}}$

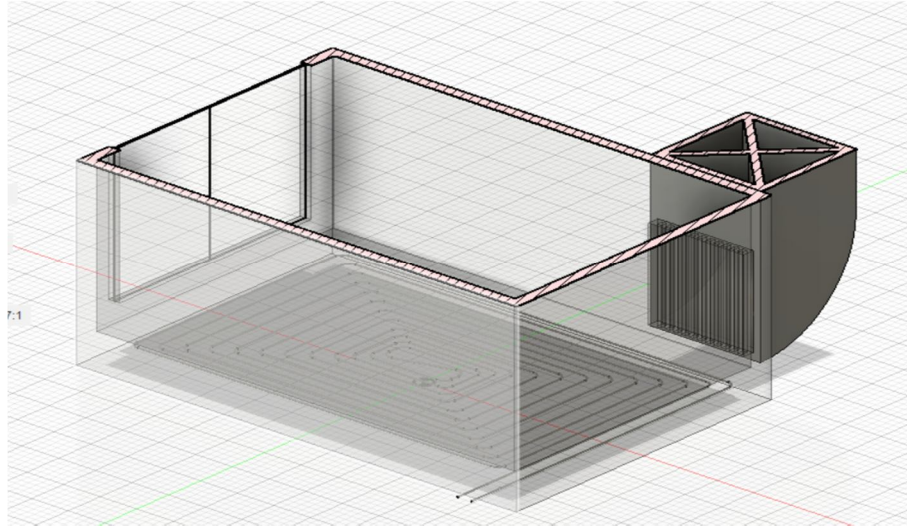


Figure .5 Radiant Cooling System

And the dimensions of the radiant cooling system are:

- 3m height
- Modulated spiral
- Pipe length= **115 m**
- Supply water temp= **9.6°C**
- Velocity = **10.68 cm/s**

D. Human Figure Analysis

The analysis of the efficiency and performance of our cooling system would be incomplete without the presence of a heat source that would be present in the use case scenario of the system. Hence the team set out to design a human-shaped source of heat emission to complete our test scenario.

However, the designs were incapable of being meshed in the analysis stage. It was attempted using open-source externally available models but achieved little to no success. Hence it was decided to approximate the shape of a human body to a sphere (Fig 3.24) and adjust the parameters that affect heat output accordingly an were able to successfully proceed with the analysis.

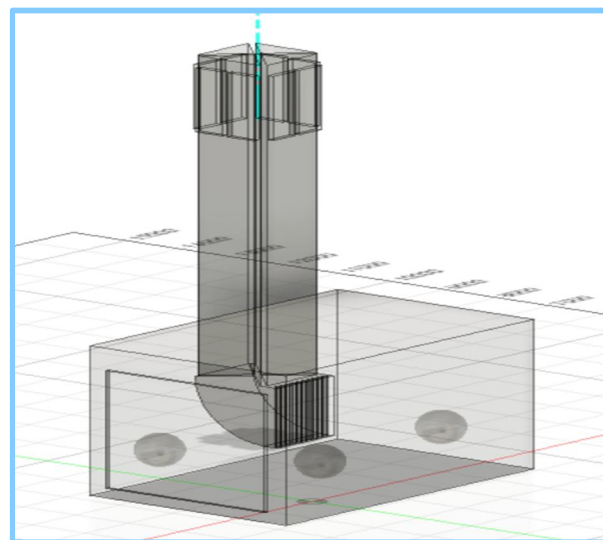


Figure .6 Room with three human spheres

The parameters used were as follows:

- Human shape: Sphere
- Sphere Diameter = **780mm** (for the average surface area of the adult human body)
- Sphere Location: **Arbitrary**
- Heat transfer coefficient = **3.4 w/m²-k**
- External emissivity = **0.96**
- Heat generation rate = **2024.875 w/m³**
- Body temperature: **36°C**

These values correspond to an average human male's statistic.

IV. RESULTS

Five separate analyses were conducted

A. Steady-state Comparison of x and k Blade Square Wind Catcher Performance

The physical dimensions used are identical for both wind catchers.

In both scenarios, the outside air temperature was **23°C** and the internal temperature was **31°C** and an identical temperature drop of **8°C** was obtained.

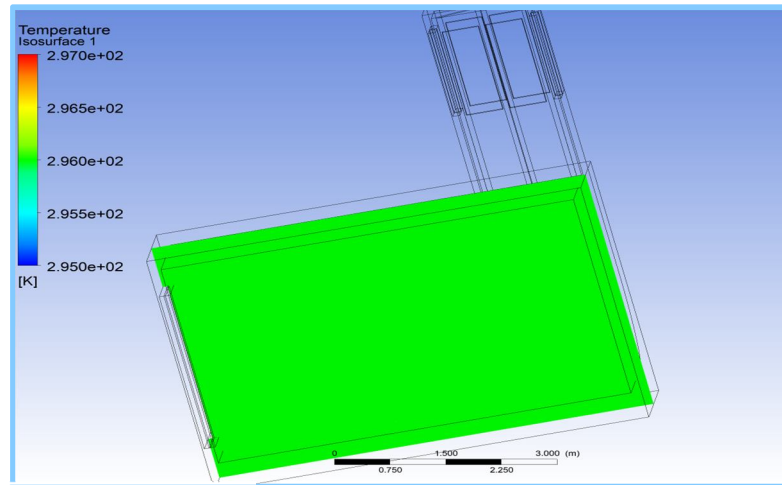


Figure .7 X-Blade Wind Catcher

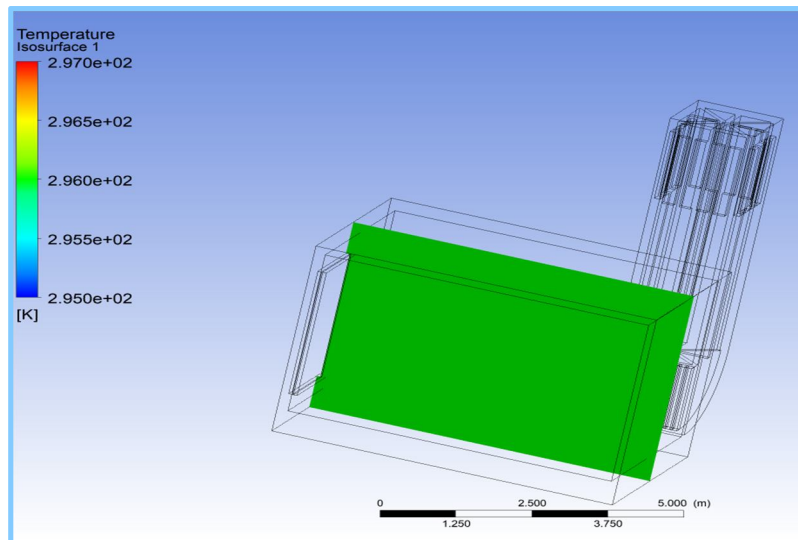


Figure .8 K-Blade Wind Catcher

B. X Blade Wind Catcher Steady-state Analysis

From the analysis, a Temperature drop of **2.7 °C** was observed in the room from **307.00K** to **304.30K**.

In time the temperature will decrease further.

In practical use, the additional airflow provided by the wind tower will provide more cooling than the numbers might suggest.

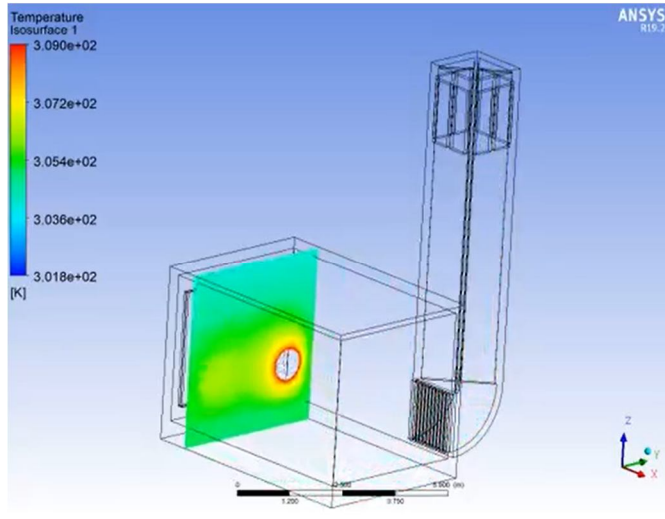


Figure .9 Steady-state Analysis of only humans radiating heat

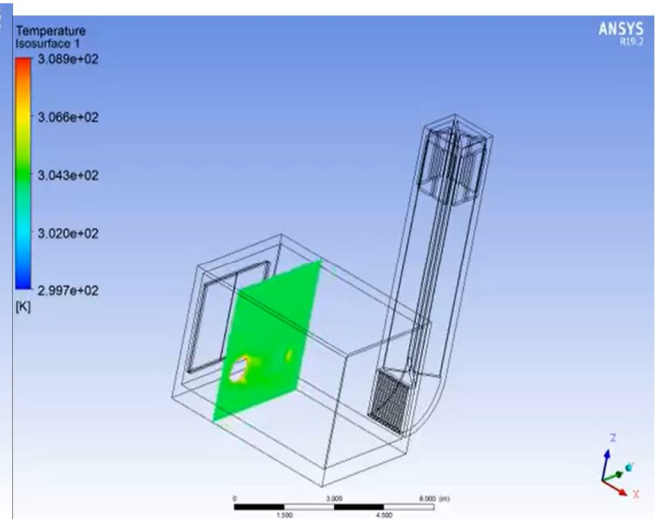


Figure .10 Steady-state Analysis of Humans radiating heat and Wind Tower cooling the room

C. X Blade Square Wind Catcher Transient State Analysis for 3m height

The room is filled with cool air in the first 10.5 seconds of the wind catcher's operation. Temperature drop and velocity increase are observed wrt time.

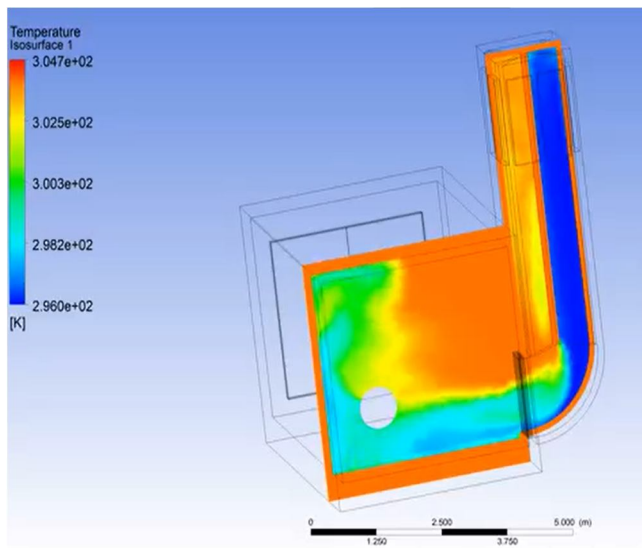


Figure .11 Transient State Analysis of 3m Wind Catcher Velocity Profile

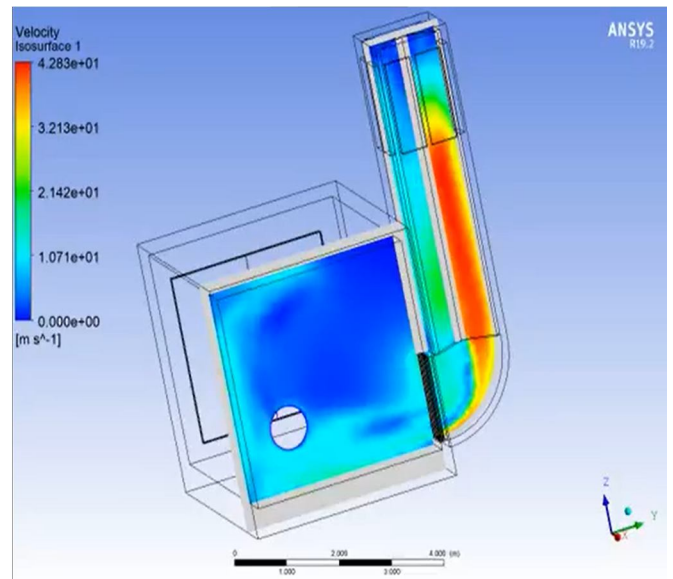


Figure .12 Transient State Analysis of 3m Wind Catcher Temperature Profile

X Blade Square Wind Catcher Transient State Analysis for 9m height

The room is filled with cool air in the first 9.2 seconds of the wind catcher's operation.

Temperature drop and velocity increases are observed wrt time.

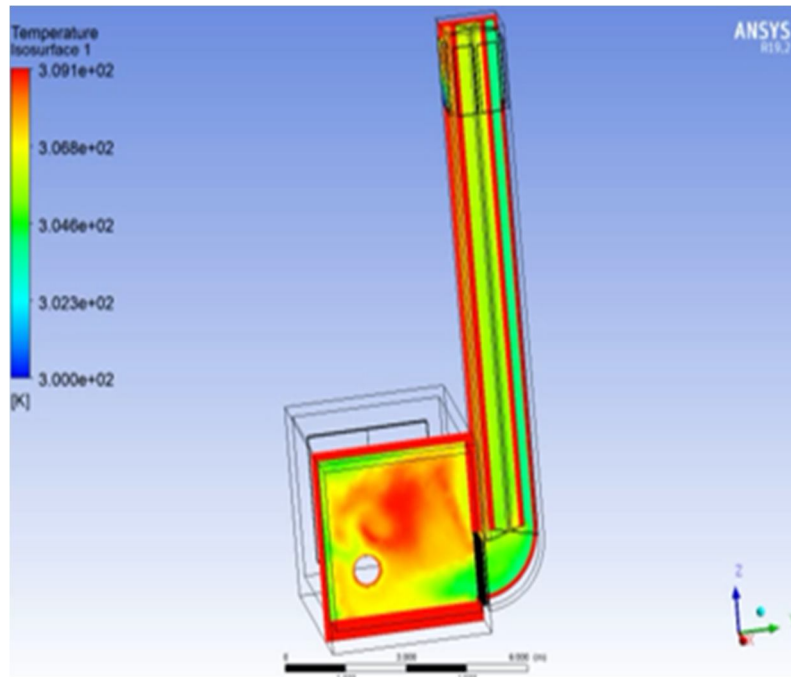


Figure 13: Transient temperature analysis for 9 m wind tower

Avg Temp vs. Time

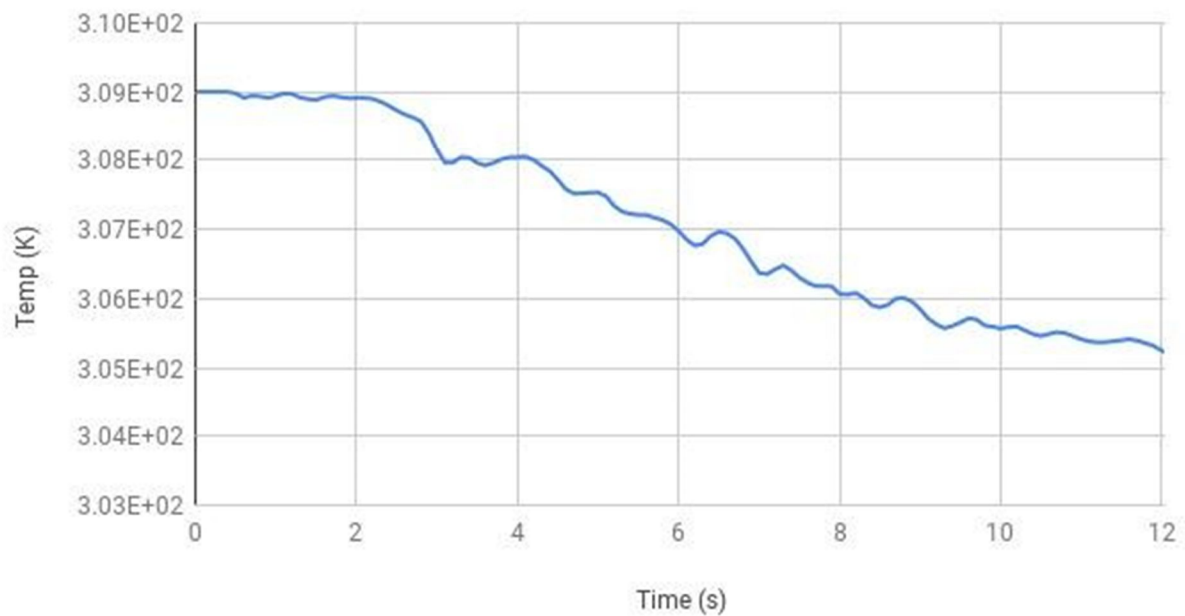


Figure 14: Temperature vs time analysis for 9m wind tower

D. Variation of temperature WRT increasing Wind Tower heights

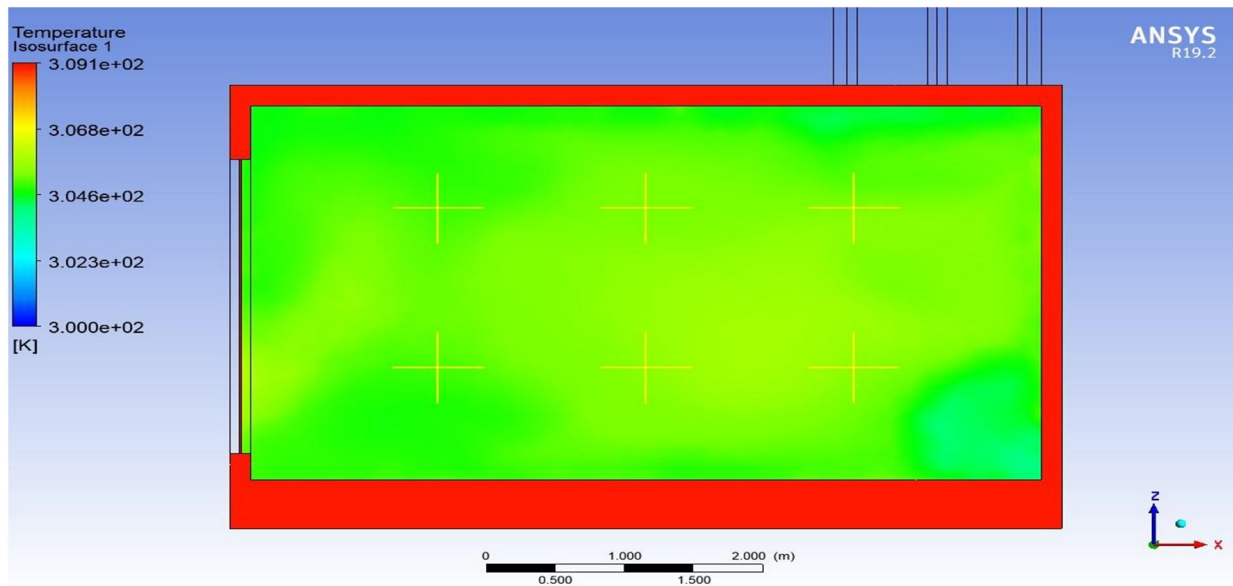


Figure 13: Six Points location on model

To conclude whether there is a relationship between increasing wind tower height and temperature drop, a steady-state analysis on the wind tower structure is conducted and measured the temperature at 6 separate locations inside the structure. A plot of the graph of the variation of temperature with respect to time at these 6 spots was generated. The variation of temperature vs time graph is shown below.

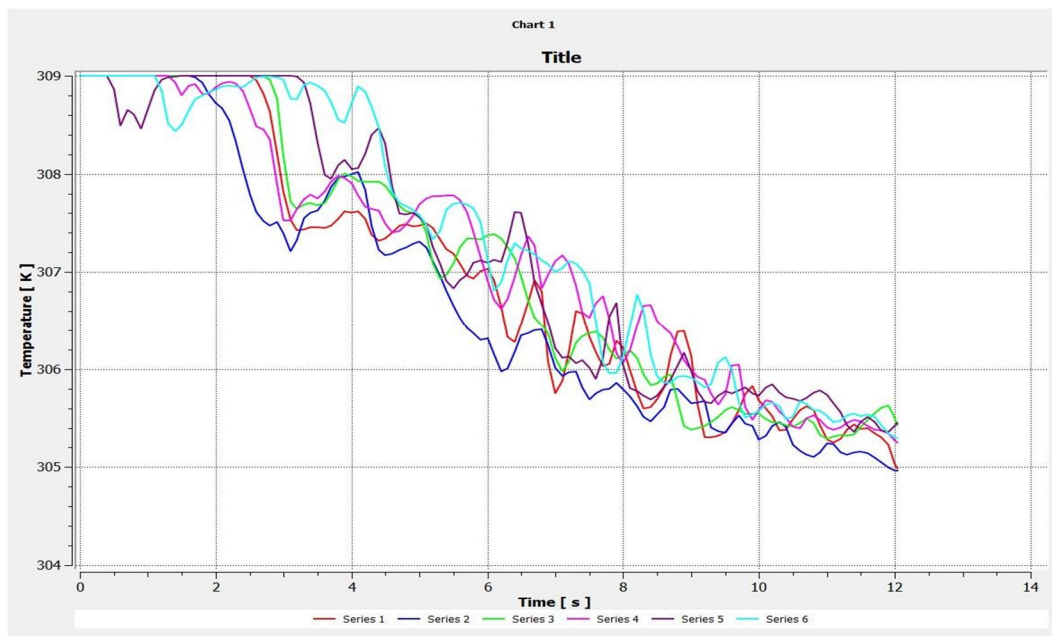


Figure 14: Temperature vs time analysis at six individual points

This experiment is then repeated for all four heights of our windcatcher and plotted the temperature is with respect to their increasing heights.

V CONCLUSION

- A. From the first analysis, it can be concluded that there is no statistical difference in performance between the x and k blade windcatcher for our experiment's climatic conditions, hence we can proceed with any design of windcatcher.
- B. From the second analysis, it can be concluded that the windcatcher mechanism is a viable method of cooling for our experiment's location and climatic conditions with sizable cooling effects.
- C. From the third analysis it can be concluded that this cooling effect occurs in a short amount of time and attains equilibrium quickly.
- D. From the fourth analysis, an increase in wind catcher height increases the rate of cooling, and a temperature drop is noticed, but a definite relationship between the wind tower's height and cooling effect cannot be determined.
- E. From the fifth analysis it can be concluded that temperature drop and by extension cooling effect is directly proportional to wind tower height.

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