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Design The Circular Water Tank by Using the STAAD Pro Software

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Abstract: Water tank are very useful for storage of water to involve the consumption of water we need to hold on to the capacity of water as much required. Now a day's storage tank are suitable for all types of environment we live as old a civilized technique. Water is the common need for all the living organisms to survive. Portable water is imperative for good health of human beings. It is most important to supply portable water to every individual and every faction; hence it is very requisite to store water. Water is generally stored in the tanks the stored water is supplied to every faction through pipelines. In the project, we have planned and designed a circular reinforced cement concrete water tank. A circular tank is manually designed. It is further analyzed using the debut analysis software STAADPRO.

I. INTRODUCTION

The form of water tanks initiate with the application parameters, hence the type of materials used and the design of water tank was control by these wavering:

- *1*) Locale of the water tank.
- 2) Volume of tank to hold water.
- *3)* What purpose the water to be used?
- 4) Temperature of locale where are the stored, have to do with for freezing.
- 5) Pressure required for the supplying water.
- 6) How con it water to be delivered to the water tank.
- 7) Wind and earthquake design considerations allow water tanks to survive seismic and high wind incidents

For the duration of history, wood, ceramic and stone has been used for the water tanks. These were all naturally eventuate and manufactured and some tanks are however in service. There are manly custom configurations that include various rectangular cubes form tanks, cone bottom and special form for specific design requirements. A functional water container should do no harm to the water is at risk of to a number of environs negative influences, as well as bacteria, viruses, algae, replace in pH, and collection of minerals. Correctly designed water tank systems work to alleviate these refusal effects.

II. DESIGN PHILOSOPHIES

This is the philosophies for the design of Structures: Working stress method Ultimate load method Limit state method.

- A. Stages in Structural Design
- 1) Planning of Structure
- 2) Drawing Study
- 3) Load Combinations
- 4) Analysis of Structures
- 5) Structural Design

III. OBJECTIVE FOR STUDY

- A. Create Modeling of the Water Tank by using the software STADDPROV8I.
- *B.* Put in the properties of water tank.
- C. Put in the different load combinations as per I.S. code
- D. Put in and designing of Water Tank.
- E. Study in location under the condition of Chhattisgarh.

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IV. LITERATURE REVIEW

Water supply system is mainly based on network of pipes by joining other components to provide a stability & balanced service. These connections networks are sometimes used underground and ground to surface. Due to the destruction of pipes constantly the soil; pipes are used manmade on the availability at the time. Failure in water supply may eventuate to surrounding soil, it increase in internal water pressure, surface traffic, Which disturbed to water supply to consumers and these cause reduction in responsibility of the system.

S.K. Khariya,(2019) 75 K.L. capacity overhead tank at village Bargaon, Block Pathatiya on 12 M. staging use the different portion are different concrete mix for economical design Water tank is the most important container to store water therefore, Crack width calculation of water tank is also necessary.

M. V. Waghmare and S.N.Madhekar, (2013) to studied conduct of tank under sloshing effect. Different specification has been considered such as height of container, bottom of water in tank (30%, 50%, 70% and full) and height of staging etc. It is notice that Sloshing of water in tank depends not only on the volume of water in tank but also on staging height and facett ratio (h/D).

V. PROBLEM IDENTIFICATION

To analyze the circular over head water tank by study of allocation in IS 3370 (2009), Double dome model of over head water tank was taken. Then it was calculating by manually through the Limit State Method. After that STAAD. Pro is used to compares the design and create the structure boost and economical by tough different dimension for same capacity tank. For easy cost prediction of tanks, this study therefore examines the cost effectiveness in terms of amount of materials and design of structure. In case of spot structure are used for working stress method because the designed structure is crack free.

VI. METHODOLOGY

To reach the objectives of the study that is to calculate and design of over head water tank using STADD PRO method, which needs the basic requirements such as safety, durability, it antiquated proposed to follow the following methodology.

- 1) Locale survey.
- 2) Geotechnical investigation.
- 3) Structural planning.
- 4) Analysis and design in STADDPRO
- 5) Detailing of the design.

VII. DESIGN COMPONENTS OF TANK

The components of R.C. Cover head circular tank. The various components of elevated tank are as follows.

- 1) Top Roof Dome The dome at top usually 100mm to 150mm thick with reinforcement along the meridian and latitudes. The rise is usually 1/5th of the span.
- 2) Ring Beam The ring beam is necessary to resist the horizontal component to the thrust of the dome. The ring beam will be designed for hoop tension induced.
- 3) Circular Wall this has to be designed for hoop tension caused due to horizontal water pressure and to resist bending moment induced to wall by liquid load.
- 4) Bottom Slab this will be designed for total load above it. The slab will also be designed for the total load above it. The slab will also be designed as a slab spanning in both directions.
- 5) Bottom Beams the bottom beam will be designed as continuous beam to transfer the entire load above it to the columns

A. Staging Portion

Columns &Braces

- 1) Columns: These are to be designed for the total load transferred to them. The columns will be braced at intervals and have to be designed for wind pressure and seismic loads which ever govern.
- 2) *Braces:* The braces are the members connecting the columns at intermediate height to columns. It is provided in slender columns to increase the column's load carrying capacity
- *3) Foundation:* As per IS: 11682-1985, a combined footing or raft footing with or without tie beam or raft foundation should be provided for all supporting columns



- *B.* Design Data Using In Water Tank Assuming Data
- 1) Capacity of water tank 1.50 Lakhs Liters
- 2) Staging of height in water tank 15.00M.
- 3) Size of water tank Ø 7.00 M. Height 4.00M.
- 4) Free Board 0.10M.
- 5) Rise of Top Dom 30*
- 6) 1 person is use water 135LPCD
- 7) Design for 1000Person
- 8) Thickness of Bottom slab 0.18M.
- 9) Thickness of Top Dom 0.10M.
- 10) Thickness of Cylindrical wall 0.15M.
- 11) Top Ring beam 0.23 x 0.23M.
- 12) Bottom Ring beam 0.30 x 0.60M.
- 13) Column size 0.35 x 0.35M.
- 14) Braising size 0.23 x 0.30M.
- 15) Parapet wall thickness 0.125 M. x height 1.2M.

VIII. MANUAL DESIGN OF ELEVATED CIRCULAR WATER TANK

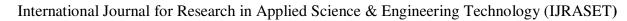
- 1) Step-1. Basic dimensions of tank: -
 - 1. Assume diameter of tank = 7m.
 - 2. Rise of top dome $(h_1) = D/7 = 7/7 = 1m$.
 - 3. Height of cylindrical wall(h_2) = 2D/5=2 x 7/5= 2.8m. ~ 4m.
 - 4. Height of conical dome $(h_3) = D/7 = 7/7 = 1m$.
- 2) Step-2. Calculate the volume of tank:

Volume of circle = $\pi r^2 h$ 150= $\pi x 3.5^2 x h$ h=150/($\pi x 3.5^2$) = 3.89 m. add free bord =1.1m. total height =4m.

- 3) <u>Step-3</u>. Design of top Dome
 - 1. Meridional force: -

$$\begin{split} T_1 &= WR_1 / (1 + \cos \Theta) \\ R_1 &= \{ (D/2)^2 + h_1^2 \} / 2 \ x \ h_1 &= \{ (7/2)^2 + 1^2 \} / 2 \ x 1 \\ &= 6.625 \sim 7m. \\ Sin\Theta &= B/H = D/2/R_1 = 7/2/7 = 0.5 \\ \Theta &= 30^* \\ Sin\Theta &= 0.5 \\ \cos\Theta &= 0.866 \end{split}$$

thickness of top dome is assumed 0.1m Dead load =2.5 KN/M² Live load =1.5 KN/M² Total load = 4 KN/M² $T_1 = 4 x7/(1+0.866) = 15$ KN/M. Meridional stress = P/A =15/(1000 x 100) = 0.15 KN/MM²





Hoop Tension: -2. a. $T_2 = WR_1[COS \Theta - (1/(1+COS \Theta))] = 4 \times 7 [0.866 - (1/1+0.866)] = -8.08 \text{ KN/M}$ Hoop stress = $P/A = 8.08 \times 10^3 / 1000 \times 100 = 0.0808 \text{ N/MM}$ 0.0808<8 Hence the design is ok. Providing minimum reinforcement 0.3% in circumferential and radial direction. $A_{st} = 0.3 \text{ x } 1000 \text{ x } 100 / 100 = 300 \text{ mm}^2$ Providing 8mm Φ bar Spacing = $(\pi/4)$ d² x 1000/ A_{st} = $(\pi/4)$ 8² x 1000/ 300 = 167.55mm Providing $_{8}$ mm Φ bar (a) 160mm c/c (A_{st} = 314.15mm²) 4) Step -4. Design of top ring beam (B_1) Horizontal component of meridional force (T): $W_1 = T_1 \cos \Theta = 15 \times 0.866 = 12.99 \text{ KN/M} \sim 13 \text{ KN/M}$ Total hoop tension on beam (T) = W x D /2 = 13 x7 /2 = 45.5 KN A_{st} for hoop tension = $T/\sigma_{st} = 45.5 \times 10^3 / 130 = 350 \text{mm}^2$ Providing 12 mm Φ bar Spacing = $(\pi/4)$ d² x 1000/ A_{st} = $(\pi/4)$ 12² x 1000/ 350 = 323.13mm Providing $_{12}$ mm Φ bar @ 200mm c/c (A_{st} = 565mm²) Stress at comprasion zone: $\sigma_{\rm ct} = \frac{T}{Ag + (m-1)Ast}$ let width assume 230 mm $1.3 = \frac{45.5 \, X \, 1000}{230 \, XD + (10 - 1)350}$ D= 138.47mm Providing size of the top ring beam is 230 x 230 mm Double shear providing 8 mm Φ bar two legged stirrups $S_{vertical} = \frac{0.87 fyAsv}{0.4 b}$ Asv (area of vertical stirrups) = $2 x \frac{\pi}{4} x 8^2 = 100 \text{ mm}^2$ $S_v = \frac{0.87 X 415 X 100}{0.4 X 230} = 392.59 \text{mm}$ Providing 8 mm Φ bar two legged stirrups @ 161mm c/c 5) Step-5. Design of Cylindrical Wall 1. Hoop tension $(T_2) = \gamma_w x h_2 x \frac{D}{2} = 9.81 x 4x \frac{7}{2} = 137.34 \text{KN}$ $A_{st} = T/\sigma_{st} = \frac{137.34 X 1000}{130} = 1056.461 \text{ mm}^2$ Area of face = $A_{st}/2 = 1056.461/2 = 528.23$ mm² Providing 12mm Φ bar @120 mm c/c Thickness of wall: -_____T $\sigma_{\rm ct} = \frac{1}{Ag + (m-1)Ast}$ a. $= \frac{137.34 X 1000}{1000 Xt + (10-1)1056.46}$ t = 94.97mm~100 mm Distribution steel: - $A_{st} = \frac{0.3 X 1000 X 100}{100} = 300 \text{ mm}^2$ Providing 8 mm Φ bar @160 mm c/c



Step-6. Design of spherical bottom dome 6) Assume thickness of dome is 0.18m Meridional force $T_3 = \frac{WR}{1 + cos\theta}$ Weight of water = $\gamma_w x h = 9.81 x 4 = 40 \text{KN/M}^2$ Self-weight = $0.18 \times 25 = 4.5 \text{KM/M}^2$ Total loads = 44.5 KN/M^2 $R_2 = \left(\frac{D^{\circ}}{2}\right)^2 + h_2^2 / (2 \ge h_2) = \left(\frac{6.8}{2}\right)^2 + \frac{1^2}{2} (2 \ge 1)$ = 6.8m. $\sin\Theta = 0.5$ Θ= 30* $T_3 = \frac{44.5 X 6.8}{1+0.866} = 162.165 \text{ KN/M}$ Meridional stress $= \frac{P}{A} = \frac{162.165 \times 1000}{1000 \times 100} = 0.9$ a. 0.9 < 8 Hence the design is ok Providing minimum % of steel 0.3% $A_{\rm st} = \frac{0.3 \, X \, 1000 \, X \, 180}{100} = 540 \, \rm{mm}^2$ Providing 10mm Φ bar @ 140mm c/c (A_{st} = 560mm²)

7) Step-7. Design of bottom ring beam

- 1. Out word thrust for bottom beam $T_3 \cos\Theta = 162.165 \times 0.866 = 140.434 \text{ KN/M}$
- 2. Hoop tension on beam $=\frac{WXD}{2} = \frac{140.434 X 7}{2}$ = 491.519 KN

3. Hoop stress $= \frac{P}{A} = \frac{491.519 \times 1000}{300 \ 600} = 2.73 \text{ N/mm}^2$

73	< 8	
2.75	10	

Hence the structure is safe.

Total load on beam: -Vertical load on beam: $= T_2 \sin \Theta_1 + T_3 \sin \Theta_2$ $= 137.34 \ge 0.5 + 162.165 \ge 0.5$ = 135b KN/M Self-weight of beam = $0.3 \times 0.6 \times 25 = 4.5 \text{ KN/M}$ Load of bottom dome = $0.18 \times 25 = 4.5 \text{ KN/M}$ Total UDL load = 135 + 4.5 + 4.5 + 144KN/M Total load $=\frac{\pi}{D}XUDL = \frac{\pi}{7}X$ 144 = 3166KN Maximum negative bending moment at support = $C_1 WR^2$ (2 Θ) Assumed Number of supports 8 = 0.066 x 144 x 3.5^2 x $\frac{\pi}{4}$ = 91.439 KN.M Maximum Positive bending moment at support = C_2WR^2 (2 Θ) $= 0.03 \text{ x } 144 \text{ x } 3.5^2 \text{ x } \frac{\pi}{4} = 41.56 \text{ KN.M}$ Maximum torsional moment at support = C_3WR^2 (2 Θ) $= 0.005 \text{ x } 144 \text{ x } 3.5^2 \text{ x } \frac{\pi}{4} = 6.92 \text{ KN.M}$ Maximum shear force at support = $\frac{W}{2 \times No. columns} = \frac{3166}{2 \times 8} = 197.8 \text{ KN}$



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Calculate Depth of beam $M = Qbd^2$ $197.87 = 2.85 \times 300 \times d^2$ D = 468.91 mm Providing depth of beam 550mm and 50 mm cover total depth 600mm $A_{st} = \frac{M}{\sigma st X j X d} = \frac{197.87 X 1000000}{130 X 0.86 X 550} = 3217.92 \text{ mm}^2$ Providing 28 mm Φ bar 6 No. @158 mm c/c Check for shear (IS:2000 pg.No.83 / IS 3370 part-2 table No. 3) $\mathbf{\overline{U}}_{v} = \frac{M}{bxd} = \frac{197.87 \times 1000}{300 \times 550} = 1.19 \text{ N/mm}^{2}$ Percentage of steel (Pt) = $\frac{100 XAst}{bXd} = \frac{100 X 3217.92}{300 X 600} = 0.019$ $\mathbf{T}_{\rm c} = \frac{0.75 - 0.19}{0.75 - 100} = \frac{0.36 - x}{0.36 - 0.4}$ $T_{c}=0.4$ **Շ**_v≻Շ_c It is design for shear Shear taken by concrete = $0.35 \times 300 \times 550 = 57.75 \text{ KN}$ Net shear force = 197.87-57.75 = 140.06 KN Provide $10\text{mm}\,\Theta$ bar 4 legged vertical stirrups. Area of vertical steel (A_{sv}) = 4 x $\frac{\pi}{4}$ x d² = 4 x $\frac{\pi}{4}$ x 7² = 314.15 mm² S_v = $\frac{AsvX\sigma svXd}{Vs} = \frac{314.15 X 175 X 550}{140.06} = 215.88$ mm Provided 10 mm Θ Bar 4 legged vertical stirrups @200 mm c/c Column details: Total bear load on column = 3166KN Dead load of the column = $0.35 \times 0.35 \times 25 \times 15$ = 45.93 KN Total dead weight of the column = 45.93×8 = 367.5Total load on column = 3166 + 367.5 = 3533.5 KN Load of 1 column = 3533.5/8 = 441.68 KN Providing 20mm Φ bar 150mm c/c $(A_{st} = 47123.88 \text{ mm}^2)$ Seismic load from IS 1893:2002 Response spectrum method For RC $T_u = 0.75 h^{0.75}$ Horizontal seismic coefficient $A_n = \frac{ZI}{2} \times S_a/g$ T<0.1S it is given from table No.2 Z = zone factor II = 0.1R = response factor = 3 To 5 = 5 from table No.7I = Impact factor = 1.5 From Table No.6 $S_a/g = soil classification$ Base shear $(V_b) = A_n \times W$ Wind load: $P_z = 0.6 V_z^2$ $V_z = V_b x K_1 x K_2 x K_3 x K_4$ V_{b} = basic wind speed = 39 in Chhattisgarh from IS 875 part III K_1 = Probability factor = 1.06 from table-1 K_2 = Terrain roughness and height factor = 0.97 from table -2



- K_3 = Topography factor = 1 K_4 = Importance factor = 1 V_z = 40.0998
- $P_z = 24.059 \text{ m/s}$

IX. DESIGNING OF CIRCULAR WATER TANK IN STAADPRO

A. Procedure

Open STAAD.pro.

Click on new project > add file name>Select 'space'.

Length (in m), Force (in KN).

choose add beam choice and click on finish.

Go to Geometry>Run structure wizard > choose surface/plate model > cylindrical surface. shut it to transfer to modelling Length :3

Division on length: one

Start radius: 3.5

Division on periphery: 8(column)

End radius: 3.5

victimisation Add beam choosing prime node and bottom node.

Repeat on outer boundary for needed variety of columns.

Copy all vertical members victimisation ctrl + C and paste aside victimisation ctrl + V.

Add intermediate nodes on length to feature required variety of beams in horizontal direction.

Connect all node in a very plane to make a circular beam.

Repeat an equivalent method at prime to urge circular beam.

Geometry>Run structure wizard> choose surface/plate model >Spherical cube choose spherical cap (Bottom dome).

shut it to transfer to modelling Diameter of sphere: Base Diameter:

Shift the obtained Spherical cap to prime beam Measure distance victimisation 'display node

to node distance' tool Select all plates > Right click mouse>Move > add (-) sign to {above|higherthan|on prime of} distance to rest on top beam.

• Geometry>Run structure wizard > choose surface/plate model > cylindrical surface

Length: 19

Division on length: one

Start radius3.5

Division on periphery:

End radius: a pair of 3.5

• Shift the obtained conelike dome to prime beam Measure distance victimisation 'display node to node distance' tool Select all plates > Right click mouse>Move > add

(-) sign to {above|higherthan|on prime of} distance to rest on top beam.

• Geometry>Run structure wizard > choose surface/plate model > cylindrical surface

Length: 15

Division on length: one

Start radius: 3.5

Division on periphery:

End radius: a pair of.5

- Shift the obtained cylindrical surface to prime beam live distance victimisation 'display node to node distance' tool Select all plates > Right click mouse>Move > add
 - (-) sign to {above|higherthan|on prime of} distance to rest on top beam.
- Geometry>Run structure wizard> choose surface/plate model >Spherical cube choose spherical cap (Top dome).
 shut it to transfer to modelling
 Diameter of sphere:
 - Base Diameter:



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- Shift the obtained conic dome to high beam live distance exploitation 'display node to node distance' tool choose all plates > Right click mouse>Move > add
 - (-) sign to {above|higherthan|on high of} distance to rest on top beam.
 - Finally Check dimensions of tank exploitation 'display node to node distance' tool to verify. Any corrections to be created area unit corrected.

B. General Properties

Click 'property' at left of screen> outline needed dimensions for individual components. Assign the property for numerous components exploitation any of the options gift per your convenient.

Click 'Support' > produce >Select 'fixed' >click Add> assign inside a part of beam.

CLICK 'LOAD AND DEFINITION'

To apply wind load initial, we've to outline it in initial section.

Enter your values. Keep exposure as -1.

Click 'Load case details' to feature metric capacity unit, LL & WL.

Add self-weight as metric capacity unit Add Water load as LL Add Wind Load Select material as concrete and assign for entire tank

C. Analysis

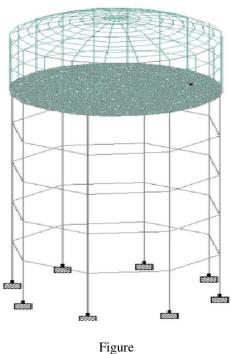
Click 'Analysis and print'> Run analysis >Check for Zero errors>Post process Apply given masses to ascertain deflected form of structure, beam moments and forces.

X. DESIGN

Click on 'Design' >Select parameters to incorporate in our design.

Define parameters with various values Select the specified command to instruct software package to design in keeping with IS code. Detailing of reinforcement and amount of concrete is gift in computer file.

A. Modeling Of The Tank

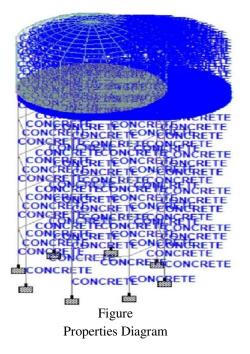


Molding Diagram



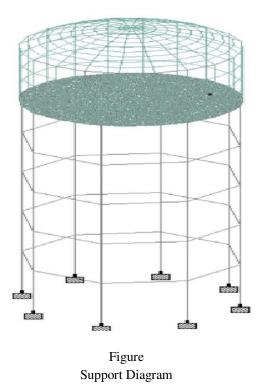
B. Assigning The Material

As after creating the beams and columns we will assign material to them as we require. Our design is concrete design hence we have assigned the concrete material to the beams and columns.



C. Specifying Supports

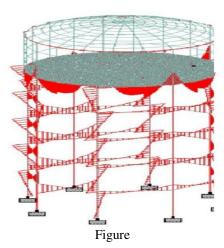
The supports are first created (as we created fixed supports) and then these are assigned to all the lowermost nodes of structure where we are going to design the foundation.



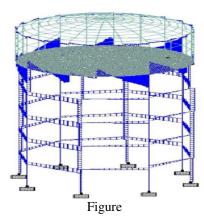


A. Bending Moment

XI. RESULTS



B. Shear Force

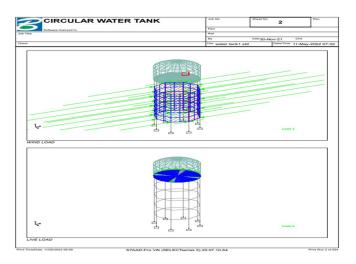


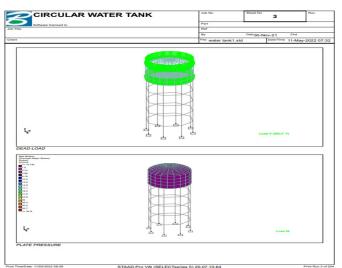
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Ali Type Primary P	The Who is printout a b b b b b b b b b b b b b b b b b b b	le Structure re results AC 1 2 2 4 4 5 6 6 7 7 9 9 10 11 12 13 14 15 16 17 16 17 16 17 20 20 20 20 20 20 20 20 20 20	w Ne SX Ne SZ SZ SZ <t< td=""><td>N CODE GENRAL SI N CODE GENRAL SI</td><td></td><td></td><td></td><td></td></t<>	N CODE GENRAL SI N CODE GENRAL SI				
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2) Loads Acting On A Structure





3) Loas Case

	CIRCULA	R WAT	TER TA	NK		Job No		Sheet No	4	Rev
	dware licensed to					Part		<u> </u>		_
Sc.	offware licensed to					Ref				
						By		Date 30-No		Chid
						File WD	iter tank1.std	0	Date/Time 1	1-May-2022 0
Code	Direction X Seismic Direction Z C Wind Le Type	Factor 1.000	a							
× ×	: Wind L	1.000 -1.000								
× 4 WZ	: Wind Lo	-1.000								
×	: Wind Lo	-1.000								
× 4 WZ	: Wind Lo	-1.000 Dading								
× 4 WZ	: Wind Lo	-1.000								
X 4 WZ Directio	Type	-1.000 Dading Factor 1.000 -1.000	Fa	Da	Fb	Оь	Ecc.	1		
X Directio Z 5 DL Beam		-1.000 Dading Factor 1.000 -1.000 Direction Direction	1.00	(m)	1000	0.000	(m)]		
X 4 WZ Directio Z Z 5 DL Beam 89		-1.000 Dading Factor 1.000 -1.000 Direction GY	-3.125	(m)	-		(m)]		
X Directio Z 5 DL Beam 89 90		-1.000 Factor 1.000 -1.000 -1.000 -1.000 Direction GY GY	-3.125 -3.125	(m) - -			(m) -			
x 4 WZ Directio Z 5 DL Beam 89 90 91		-1.000 Factor 1.000 -1.000 Direction GY GY GY	-3.125 -3.125 -3.125	(m)	-		(m)			
X Directio Z Z 5 DL Beam 89 90 91 92	1	-1.000 Factor 1.000 -1.000 -1.000 Direction GY GY GY GY GY	-3.125 -3.125 -3.125 -3.125	(m) - -		-	(m) - -			
x 4 WZ Directio Z 5 DL Beam 89 90 91		-1.000 Factor 1.000 -1.000 Direction GY GY GY	-3.125 -3.125 -3.125	(m) - - -		-	(m) - -			
x 4 WZ Directio 2 5 DL 8eam 89 90 91 92 93 94	1	-1.000 Pactor Factor 1.000 -1.000 -1.000 Direction GY GY GY GY GY GY	-3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125	(m) - - -		-	(m) - -			
x 4 WZ Directio 2 5 DL Beam 80 90 91 92 93	1 : Wind Lo in Type 1 1 : Beam Lo Type UNI KNNm	-1.000	-3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125	(m) - - - - -			(m) - - - - -			
x Directio Z 5 DL Beam 89 90 91 92 93 94 95	1	-1.000 Pactor Factor 1.000 -1.000 -1.000 Direction GY GY GY GY GY GY	-3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125	(m) - - - - -			(m) - - - - - -			
x 4 WZ Directio 2 5 DL 8 eam 8 9 90 91 92 93 94 95 96	1	-1.000 Pactor 1.000 -1.000 -1.000 -1.000 Direction GY GY GY GY GY GY GY GY GY G	-3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125	(m) - - - - - - -			(m) - - - - - - -			
x 4 WZ Directio Z 5 DL 8 9 90 91 92 93 94 95 96 97	1 : Wind Lc m Type 1 1 : Beam Lc Type UNI KNNm	-1.000	-3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125	(m) - - - - - - - - - -			(m) 			
x 4 WZ Direction Z Z 5 DL 8 eam 890 911 92 93 94 95 96 97 98	1	-1.000 Pading Factor 1.000 -1.000 -1.000 Direction GY	-3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125	(m) - - - - - - - - -			(m) 			
x Directio Z 5 DL Beam 89 90 91 92 93 94 95 96 96 97 98 99	1 : Wind Lc n Type 1 1 : Beam Lc UNI RNIM	-1.000	-3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125	(m) 			(m) 			
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International Journal for Research in Applied Science & Engineering Technology (IJRASET)

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C	IRCU	LA	R WAT	ER TA	NK		Job No		Sheet No 8	Rev
							Bad			
Sof	twore licensed	50					Ref			
							Dy		DeH30-Nov-21 C	
							File wat	ter tank1.std	Date/Time 11-	May-2022 07:3
eam 1558 1568 1595 1729 1744 1769 1884 1921 1921 1952 1986 1216	Type	N/m N/m N/m N/m N/m N/m N/m N/m N/m N/m	Direction GY GY GY GY GY GY GY GY GY GY	Fa -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125 -3.125	Da (m) - - - - - - - - - - - - - - - -	Fb 	Db 	Ecc. (m) - - - - - - - - - - - - - -		
238		N/m	GY	-3.125	-	-]	
239		N/m	GY	-3.125	-	· · ·			1	
356		N/m	GY	-3.125	-	-	-	-	1	
5362 5363		N/m	GY	-3.125	-	-	-	-	1	
		N/m	GY	-3.125	-				1	
377		N/m	GY	-3.125					4	
549		N/m	GY	-3.125	-		-		1	
590		N/m	GY	-3.125					1	
611		N/m	GY	-3.125					1	
487		N/m	GY	-3.125					1	
733		N/m	GY	-3.125					1	
207		N/m	GY	-3.125	-				1	
217	UNI	N/m	GY	-3.125	-			-	1	
264		N/m	GY	-3.125	-	-			1	
360	UNI	N/m	GY	-3.125	-				1	
704	UNI	N/m	GY	-3.125	-	-		-	1	
2305	UNI k	N/m	GY	-3.125	-	-			1	
2309	UNI k	N/m	GY	-3.125	-	-		-	1	
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DL :	Factor	eig	iht		ssigned G					
Culon		1		~	a signed G	connectry				
Y	-1.000	ALL							1	
Load N/mm ²] -0.00		-		(m) -	Max X (m) - Pro V8i (S8	Min Y (m) -	Max Y (m) - 5) 20.07.10.	64		Print Run 8 of
-			R WAT				ant Ne		Report No.	Rev

						Dy.		Data a s	Chil
								Date 30-No	
						Pile wat	er tank1.std		DaterTime 11-May-2022 0
EI.	: Plate Lo	ade							
Plate	Туре	Direction	Fa	FD	X1	¥1	X2	¥2	
					(m)	(m)	(m)	(m)	_
109	TRAP N/mm2	Z	-0.010	-0.011	-		-	-	_
110	TRAP N/mm2 TRAP N/mm2	Z	-0.011	-0.013				-	-
112	TRAP N/mm2	Z	-0.015	-0.016	-				-
112	TRAP N/mm2	Z	-0.020	-0.025	-		-		-
114	TRAP N/mm2	Z	-0.025	-0.029	-			-	-
114	TRAP N/mm2		-0.025	-0.029				-	-
115	TRAP N/mm2	Z	-0.029	-0.035		:		-	
116	TRAP N/mm2	Z	-0.035	-0.039	-		-		
118	TRAP N/mm2	Z	-0.039	-0.039	-		-		-1
119	TRAP N/mm2	2	-0.039	-0.039	-		-		-1
120	TRAP N/mm2	2	-0.039	-0.036	-				
121	TRAP N/mm2	Z	-0.036	-0.033	-				
122	TRAP N/mm2	Z	-0.033	-0.029					
123	TRAP N/mm2	Z	-0.029	-0.025					-
124	TRAP N/mm2	Z	-0.025	-0.020	-				-
125	TRAP N/mm2	z	-0.020	-0.016					-
126	TRAP N/mm2	Z	-0.016	-0.013	-				
127	TRAP N/mm2	Z	-0.013	-0.011	-			-	-
128	TRAP N/mm2	Z	-0.011	-0.010	-			-	-1
129	TRAP N/mm2	Z	-0.010	-0.011	-			-	-1
130	TRAP N/mm2	Z	-0.011	-0.013	-			-	-1
131	TRAP N/mm2	Z	-0.013	-0.016	-			-	-
132	TRAP N/mm2	Z	-0.016	-0.020	-			-	-
133	TRAP N/mm2	Z	-0.020	-0.025	-			-	-
134	TRAP N/mm2	Z	-0.025	-0.029	-	-		-	-
135	TRAP N/mm2	Z	-0.029	-0.033	-		-	-	_
136	TRAP N/mm2	Z	-0.033	-0.036	-	-		-	
137	TRAP N/mm2	Z	-0.036	-0.039	-			-	
138	TRAP N/mm2	Z	-0.039	-0.039	-				
139	TRAP N/mm2	Z	-0.039	-0.039	-		-	-	
140	TRAP N/mm2	Z	-0.039	-0.036	-		-	-	
141	TRAP N/mm2	Z	-0.036	-0.033	-		-	-	
142	TRAP N/mm2	Z	-0.033	-0.029	-		-	-	
143	TRAP N/mm2	Z	-0.029	-0.025	-		<u>.</u>	-	
144	TRAP N/mm2	Z	-0.025	-0.020	-	-	-	-	
145	TRAP N/mm2	z	-0.020	-0.016	-		-	-	_
146	TRAP N/mm2	Z	-0.016	-0.013	-	~		-	_
147	TRAP N/mm2	Z	-0.013	-0.011	-		-	-	_
148	TRAP N/mm2	Z	-0.011	-0.010	-		-	-	_
149	TRAP N/mm2	z	-0.010	-0.011	-		-	-	_
150	TRAP N/mm2	z	-0.011	-0.013	-		-	-	_
151	TRAP N/mm2	Z	-0.013	-0.016	-	-	-	-	_
152	TRAP N/mm2	Z	-0.016	-0.020	-		-	-	
153	TRAP N/mm2	Z	-0.020	-0.025	-	-	-	-	

	IRCULA	R WAT	ER TA	NK		Job No		Sheet No	276	Rev
						Part				
54	ftware licensed to					Ref				
									In 21 Ch	
						By		Date 30-N		
						File with	ter tank1 str	4	Date/Time 11-M	day-2022 07
FL	Type	ads Co	nt	Fb	X1	¥1	X2	Y2	_	
					(m)	(m)	(m)	(m)		
12288	TRAP N/mm2	Z	-0.026	-0.026	-	-	-	-		
12289	TRAP N/mm2	Z	-0.026	-0.026		-	-	-		
12290	TRAP N/mm2	Z	-0.026	-0.026				-		
12291	TRAP N/mm2	Z	-0.026	-0.026						
12292	TRAP N/mm2	Z	-0.026	-0.026	-	-	-	-	_	
12293	TRAP N/mm2	Z	-0.026	-0.025		-		-	_	
12294	TRAP N/mm2 TRAP N/mm2	Z	-0.025	-0.025	-	-		-		
12295	TRAP N/mm2 TRAP N/mm2	Z	-0.025	-0.024	-	-				
12296	TRAP N/mm2	Z	-0.024	-0.023	-	-		-	-	
12298	TRAP N/mm2	Z	-0.023	-0.023	-				-	
12299	TRAP N/mm2	Z	-0.023	-0.023					-	
12300	TRAP N/mm2	Z	-0.023	-0.023		-		-		
12301	TRAP N/mm2	Z	-0.023	-0.023	-	-	-	-	-	
12302	TRAP N/mm2	Z	-0.023	-0.024		-	-	-		
12303	TRAP N/mm2	z	-0.024	-0.024	-	-	-	-		
12304	TRAP N/mm2	Z	-0.024	-0.025						
12.004	•	~	-0.024	-0.025		-				



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4) Displacement

\geq	IRCI	ULAR WA	TERT	ANK		Job Pao	64	27	7	Play
	Amore Diserva.	and her				Part				
1.00						Faul				
						-	0.4	*30-Nov-21	CP-d	
						F110	or tank1.std	Literary .	THINK IS A R.C.	ay-2022 0
		Displacen								
Beam	Node	un in italic indicate	X (mm)	(mm)	(mm)	Resultant				
9		1:08	1.054	-0.041	0.000	1.055				
-		282	0.000	0.000	1.059	1.050				
		2.978	-0.295	0.001	0.000	0.295				
		4.002	0.292	-0.001	0.000	0.292				
		5.DL	-0.005	-0.206	0.000	0.206				
		GLL	-0.000	-0.007	0.000	0.007				
		2.FL 28-CENERATE	0.000	-1.030	-1.588	1.030				
	10	1.55X	1.057	-0.185	0.002	1.600				
	10	1.8×	1.057	-0.028	1.007	1.057				
		2.52	0.002	0.028	0.007	0.122				
		1.002	0.080	0.000	0.088	0.122				
		5.01	0.000	-0.150	-0.004	0.150				
		OILL	0.000	-0.004	-0.000	0.004				
		7.FL	0.136	-0.609	-0.027	0.625				
		28 GENERATE	0.000	-0.182	-7.000	1.0199				
10	10	1.658	1.057	-0.028	0.002	1.057				
		2.92	0.002	0.028	1.057	1.057				
		14.002	0.086	0.000	0.085	0.122				
		0.00	0.003	-0.150	-0.004	0.150				
		OLL	0.000	-0.004	-0.000	0.004				
		7.5%	0.136	-0.609	-0.027	0.625				
		28 GENERATE	0.000	-0.182	-1.048	1.599				
	11	1.0×	1.059	0.000	0.000	1.059				
		2.92	0.000	0.041	1.054	1.055				
		3 WX	0.000	-0.001	0.202	0.202				
		4.W2	0.000	-0.200	0.205	0.295				
	-	ell	0.000	-0.008	0.000	0.000				
		ZFL	9,112	-0.714	0.025	0.724				
		PROENEDATE	0.000	-0.240	-1.677	4.090				
11	11	1:85×	1.059	0.000	0.000	1.059				
		2:92	0.000	0.041	1.054	1.055				
		3.998	0.000	-0.001	-0 X9X	0.292				
		4.002	0.000	0.001	0.205	0.295				
		5.DL	0.000	-0.206	0.005	0.208				
		OLL 7FL	9,116	-0.000	0.025	0.006				
		28 GENERATE	0.000	-0.240	-1-977	1,000				
	12	1 TAX	1.007	0.028	-0.002	1.057				
		2.62	-0.002	0.020	1.057	1.057				

	- COU	JLAR	WATER	TANK		Job No		Sheet No	368	Rei
>	twore lisence	4.50				Part				_
0						Ref				
						By		Date 30-N	DW-21 Chd	
						File w	ater tank1.st		Date/Time 11-Ma	nr-2021
Beam	Node	Displa	cements	Cont	z	Resultant				
1.11			(mm)	(mm)	(mm)	(mm)				
		7:FL	4.384	-3.381	-0.133	5.538				
		28:GENER	ATE -0.009	-1.042	-13.111	13.153				
			4		档	Load 28 : Disp	ac amount			
Beam	n Maxi		Moments		4	Load 28 : Disp	accoment			
Beam	n Maxi	a are given t Length	Moments		d	Max My	đ	Max Mz]	
Beam	to maximi Node A	a are given t Length (m)	rom beam end A. L/C		d (m)	Max My (kNm)	d (m)	(kNm)]	
Beam	Maxim	a are given t Length	rom beam end A.	Max +ve	d (m) 0.000	Max My (kNm) 0.009	d (m) 0.000	(kNm) 4.075]	
Beam	to maximi Node A	a are given t Length (m)	rom beam end A. L/C 1:SX	Max -ve	d (m)	Max My (kNm)	d (m) 0.000 2.679	(kNm) 4.075 -3.292		
Beam	to maximi Node A	a are given t Length (m)	rom beam end A. L/C	Max -ve Max +ve	d (m) 0.000 2.679	Max My (kNm) 0.009 -0.010	d (m) 0.000 2.679 0.000	(kNm) 4.075 -3.292 8.760		
Beam	to maximi Node A	a are given t Length (m)	1:SX 2:SZ	Max -ve Max +ve Max -ve	d (m) 0.000 2.679 2.679	Max My (kNm) 0.009 -0.010 -0.007	d (m) 0.000 2.679 0.000 2.679	(kNm) 4.075 -3.292 8.760 -9.090		
Beam	to maximi Node A	a are given t Length (m)	rom beam end A. L/C 1:SX	Max -ve Max +ve	d (m) 0.000 2.679	Max My (kNm) 0.009 -0.010	d (m) 0.000 2.679 0.000	(kNm) 4.075 -3.292 8.760		
Beam	to maximi Node A	a are given t Length (m)	1:SX 2:SZ	Max -ve Max +ve Max -ve Max +ve	d (m) 0.000 2.679 2.679 0.000	Max My (kNm) 0.009 -0.010 -0.007 0.621	d (m) 0.000 2.679 0.000 2.679 2.679	(kNm) 4.075 -3.292 8.760 -9.090 0.965		
Beam	to maximi Node A	a are given t Length (m)	I:SX 2:SZ 3:WX	Max -ve Max +ve Max -ve Max +ve Max -ve	d (m) 0.000 2.679 2.679 0.000 2.679	Max My (kNm) -0.009 -0.010 -0.007 -0.007 -0.009	d (m) 0.000 2.679 0.000 2.679 0.000	(kNm) 4.075 -3.292 8.760 -9.090 0.965 -1.076		

5) Bending Moment

-	CIRCL	JLAR	WATER	TANK		Job No	>	Sheet No	460	R	tev
						Part		<u> </u>			-
So	dware license	d 90				Ref					-
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						Pile W	ater tank1.st	td	Daber Time	11-May-20	12.
Ļ.			-	- Martin	4		Load 28 : Be	inding Z			
BENDING			Shear For		14		Load 28 : Be	inding Z			
Beam	n Maxi	imum \$	Shear For	ces			Load 28 : Be	inding Z			
Beam Distances	n Maxi	a are given f	Shear For	ces		Max Fz	đ	Max Fy]		
Beam Distances Beam	Node A	a are given to Length (m)	L/C		v (m)	Max Fz (kN)	d (m)	Max Fy (kN)			
Beam Distances	n Maxi	a are given t Length (m)	rom beam end A.	Max +ve	(m)	(kN)	đ	Max Fy			
Beam Distances Beam	Node A	a are given to Length (m)	1:SX	Max +ve Max -ve			d (m) 0.000	Max Fy (kN) 2.750	1		
Beam Distances Beam	Node A	a are given to Length (m)	L/C	Max +ve	(m)	(kN)	d (m)	Max Fy (kN)	1		
Beam Distances Beam	Node A	a are given to Length (m)	nom beam end A. L/C 1:SX	Max +ve Max -ve Max +ve	(m) 0.000 0.000	(kN) -0.007 -0.002	d (m) 0.000	Max Fy (kN) 2.750 6.664			
Beam Distances Beam	Node A	a are given to Length (m)	1:SX 2:SZ 3:WX	Max +ve Max -ve Max +ve Max -ve Max +ve	(m) 0.000 0.000	(kN) -0.007 -0.002 -0.235	d (m) 0.000 0.000	Max Fy (kN) 2.750 6.664 -0.762			
Beam Distances Beam	Node A	a are given to Length (m)	1:SX 2:SZ	Max +ve Max -ve Max +ve Max -ve Max +ve Max +ve	(m) 0.000 0.000	(kN) -0.007 -0.002	d (m) 0.000	Max Fy (kN) 2.750 6.664			
Beam Beam	Node A	a are given to Length (m)	I:SX 2:SZ 3:WX 4:WZ	Max +ve Max -ve Max +ve Max -ve Max -ve Max -ve Max -ve	(m) 0.000 0.000	(kN) -0.007 -0.002 -0.235	d (m) 0.000 0.000 0.000	Max Fy (kN) 2.750 6.664 -0.762 0.762			
Beam Distances Beam	Node A	a are given to Length (m)	1:SX 2:SZ 3:WX	Max +ve Max -ve Max +ve Max +ve Max -ve Max -ve Max +ve	(m) 0.000 0.000 0.000	(kN) -0.007 -0.002 -0.235 0.235	d (m) 0.000 0.000 0.000 0.000	Max Fy (kN) 2.750 6.664 -0.762 0.762 1.849			
Beam Distances Beam	Node A	a are given to Length (m)	1:SX 2:SZ 3:WX 4:WZ 5:DL	Max +ve Max -ve Max +ve Max -ve Max +ve Max +ve Max +ve Max +ve Max +ve Max -ve	(m) 0.000 0.000	(kN) -0.007 -0.002 -0.235	d (m) 0.000 0.000 0.000	Max Fy (kN) 2.750 6.664 -0.762 0.762			
Beam Beam	Node A	a are given to Length (m)	I:SX 2:SZ 3:WX 4:WZ	Max +ve Max -ve Max +ve Max +ve Max -ve Max -ve Max +ve	(m) 0.000 0.000 0.000	(kN) -0.007 -0.002 -0.235 0.235	d (m) 0.000 0.000 0.000 0.000	Max Fy (kN) 2.750 6.664 -0.762 0.762 1.849			
Beam Beam	Node A	a are given to Length (m)	1:SX 2:SZ 3:WX 4:WZ 5:DL	Max +ve Max -ve Max +vo Max +ve Max +ve Max -ve Max +ve Max +ve Max +ve Max +ve	(m) 0.000 0.000 0.000 0.000 0.000	(kN) -0.007 -0.002 -0.235 0.235 -0.037	d (m) 0.000 0.000 0.000 0.000 0.000 2.679	Max Fy (kN) 2.750 -0.762 0.762 1.849 -2.506			
Beam Beam	Node A	a are given to Length (m)	rom beam end A. L/C 1:SX 2:SZ 3:WX 4:WZ 5:DL 6:LL 7:FL	Max +ve Max -ve Max +ve Max +ve Max +ve Max +ve Max +ve Max -ve Max -ve Max +ve Max -ve Max -ve	(m) 0.000 0.000 0.000 0.000 0.000	(kN) -0.007 -0.002 -0.235 0.235 -0.037	d (m) 0.000 0.000 0.000 0.000 0.000 2.679	Max Fy (kN) 2.750 -0.762 0.762 1.849 -2.506			
Beam Beam	Node A	a are given to Length (m)	rom beam end A. L/C 1:SX 2:SZ 3:WX 4:WZ 5:DL 6:LL	Max +ve Max -ve Max +ve Max +ve Max -ve Max -ve Max +ve Max +ve Max +ve Max -ve Max -ve Max -ve Max +ve Max +ve	(m) 0.000 0.000 0.000 0.000 0.000 0.000	(kN) -0.007 -0.002 -0.235 0.235 -0.037 -0.037 -0.002 -0.261	d (m) 0.0000 0.0000 0.0000 0.0000 0.0000 2.679 0.0000 0.0000	Max Fy (kN) 2.750 6.664 -0.762 0.762 1.849 -2.506 -0.015 -2.299			
Beam Beam	Node A	imum S a are given h Length (m) 2.679	rom beam end A. L/C 1:SX 2:SZ 3:WX 4:WZ 5:DL 6:LL 7:FL	Max +ve Max -ve Max +ve Max +ve Max +ve Max +ve Max +ve Max -ve Max -ve Max +ve Max -ve Max -ve	(m) 0.000 0.000 0.000 0.000 0.000	(kN) -0.007 -0.002 -0.235 0.235 -0.037 -0.002	d (m) 0.000 0.000 0.000 0.000 0.000 2.679 0.000	Max Fy (kN) 2.750 6.664 -0.762 0.762 1.849 -2.506 -0.015			

STAAD.Pro V8i (SELECTseries 5) 20.07.10.64

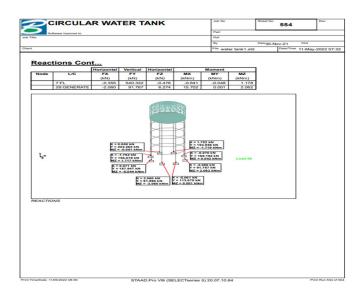


6) Shear Force

20	IRCULA	R WAT	ER T	ANK		200 140		Sheet No	552		Rev
~	dware toensed to					Part					-
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							er tank1.std		Date/Time		
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Ŀ	ORCE		ľ				Lines 20 - Se				
L- HEAR P	tions				4		Louis 28 - Br	hear Y			
Reac	tions	Horizontal	Vertical	Horizontal	4	Moment		1			
		Horizontal FX (kN)	Vertical	Horizontal		Moment MY	MZ (RVm)	1			
Reac	tions	FX	FY	FZ		MY	MZ]			
Node	tions	FX (kN)	(KN)	FZ (kN)	(kNm)	(kNm)	MZ (kNm)]			
Node	L/C	FX (kN) -3.007	FY (kN) 36.143 -0.019 -0.836	FZ (kN) 0.000 -5.571 -0.000	(kNm) 0.001 -11.858 -0.000	MY (kNm) 0.001 0.012 -0.000	MZ (kNm) 9.313 -0.001 -2.966				
Node	L/C 1:5X 2:52 3:WX 4:WZ	FX (kN) -3.007 0.000 1.206 -1.192	FY (kN) 36.143 -0.019 -0.836 0.832	FZ (kN) 0.000 -5.571 -0.000 0.000	(kNm) 0.001 -11.858 -0.000 0.000	MY (kNm) 0.001 0.012 -0.000 0.000	MZ (kNm) 9.313 -0.001 -2.960 2.930				
Node	L/C 118X 2:9Z 3:WX 4:WZ 6:DL	FX (kN) -3.007 0.000 1.206 -1.192 -0.077	FY (kN) 36.143 -0.019 -0.836 0.832 186.848	F2 (kN) -5.571 -0.000 -0.000 -0.000	(kNm) 0.001 -11.858 -0.000 0.000 -0.001	MY (kNm) 0.001 0.012 -0.000 0.0000 -0.001	MZ (kNm) 9.313 -0.001 -2.966 2.930 0.046				
Node	L/C 115X 2:52 3:WX 4:WZ 5:0L 6:LL	FX (kN) -3.007 0.000 1.206 -1.192 -0.077 0.004	FY (kN) 36.143 -0.019 -0.836 0.832 186.848 5.758	FZ (kN) -5.571 -0.000 -0.000 -0.000 -0.000	(kNm) 0.001 -11.858 -0.000 0.000 -0.001 -0.000	MY (kNm) 0.001 0.012 -0.000 0.000 -0.001 -0.000	MZ (kNm) 9.313 -0.001 -2.960 2.930 0.046 -0.005	haar V			
Node	L/C 1:8X 2:92 3:WX 4:WZ 5:DL 6:LL 7:FL	FX (kN) -3.007 0.000 1.206 -1.192 -0.077 0.004 0.583	FY (kN) 36.143 -0.019 -0.836 0.832 186.848 5.758 918.427	FZ (NN) -5.571 -0.000 -0.000 -0.000 -0.000 -0.000	(kNm) 0.001 -11.858 -0.000 0.000 -0.001 -0.001 -0.000 -0.004	MY (k.Nm) 0.001 0.012 -0.000 -0.000 -0.001 -0.000 -0.004	MZ (kNm) 9.313 -0.001 -2.966 2.930 0.046 -0.005 -0.162				
Node 1	L/C 1/8X 2:9Z 3:WX 4:WZ 5:DL 6:LL 7:FL 28:GENERATE	PX (NN) -3.007 0.000 1.206 -1.192 -0.077 0.004 0.583 -0.070	FY (NN) 366.143 -0.019 -0.836 0.832 186.848 5.758 918.427 168.192	FZ (NN) 0.000 -5.571 -0.000 -0.000 -0.000 -0.000 8.356	(kNm) 0.001 -11.858 -0.000 0.000 -0.001 -0.000 -0.004 17.786	MY (kNm) 0.001 0.012 0.000 0.000 -0.001 -0.000 -0.004 -0.018	MZ (kNm) 9-313 -0.001 -2.066 2.030 0.046 -0.005 -0.062 0.042				
Node	L/C 1:8X 2:92 3:WX 4:WZ 5:DL 6:LL 7:FL 28:GENERATE 1:8X	FX (NN) -3.007 0.000 1.206 -1.192 -0.077 0.004 0.583 -0.070 -4.286	FY (kN) 36.143 -0.019 -0.836 0.832 186.848 5.758 918.427 168.192 24.375	FZ (NN) -0.000 -5.571 -0.0000 -0.000000 -0.0000 -0.0000 -0.0000 -0.0000 -0	(kNm) 0.001 -11.858 -0.000 0.000 -0.001 -0.001 -0.004 17.786 -1.259	MY (kNm) 0.001 0.012 -0.000 -0.000 -0.001 -0.000 -0.004 -0.018 -0.000	MZ (kNm) 9.313 -0.001 -2.060 0.046 -0.005 -0.162 10.585				
Node 1	tions 1.8x 2.92 3.90X 4.90Z 5.0L 6.LL 7.FL 26.GENERATE 1.8X 2.8Z	FX (kN) -3.007 0.000 1.206 -1.192 -0.077 0.004 0.583 -0.070 -4.286 -1.270	FY (kN) 36.143 -0.019 -0.836 0.832 186.848 5.758 918.427 168.192 24.375 -24.359	FZ (kN) 0.000 -5.571 -0.000 -0.000 -0.000 -0.002 8.356 -1.270 -4.286	(kNm) 0.001 -11.858 -0.000 0.000 -0.001 -0.000 -0.004 17.786 -1.259 -10.583	MY (kNm) 0.001 0.012 -0.000 -0.000 -0.000 -0.004 -0.018 -0.008 -0.000	MZ (kNm) 9.313 -0.001 2.996 2.930 0.046 -0.005 -0.162 0.042 0.042 10.588 1.280				
Node 1	tions 1/8X 2/9Z 3/9X 4/97 4/97 4/97 4/97 4/97 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 20	FX (kN) -3.007 0.000 1.206 -1.192 -0.077 0.004 0.583 -0.070 -4.286 -1.270 0.550	FY (kN) 366.143 -0.019 -0.836 0.832 186.848 5.758 918.427 168.192 24.375 -24.359 -0.002	FZ (kN) 0.000 -5.571 -0.000 -0.000 -0.000 -0.000 -0.000 8.356 -1.270 -4.286 0.521	(kNm) 0.001 -11.858 -0.000 0.000 -0.000 -0.004 -0.004 17.786 -1.259 -10.583 1.005	MY (kNm) 0.001 0.012 0.000 0.000 -0.000 -0.000 -0.000 -0.004 -0.018 -0.000 -0.000 -0.000 -0.000 -0.000	MZ (kNm) 9.313 -0.001 -2.906 0.046 -0.065 -0.652 0.042 10.685 1.280 -1.059				
Node 1	L/C 15X 2.52 3.WX 4.WZ 5.DL 6.LL 7.FL 28.GENERATE 1.252 2.52 3.WX 4.WZ	FX (kN) -3.007 0.000 1.206 -1.102 0.004 0.583 -0.077 -0.070 -4.286 -1.270 0.530 -0.521	FY (kN) 36.143 -0.019 -0.836 0.832 186.848 5.758 918.427 168.192 24.375 -24.359 0.002 0.002	FZ (kN) -5.571 -0.0000 -0.0000	(kNm) 0.001 -11.858 -0.000 0.000 -0.001 -0.004 17.786 -1.259 -10.583 1.025	MY (kNm) 0.001 0.012 -0.000 -0.000 -0.000 -0.004 -0.018 -0.000 -0.000 -0.000 -0.000 -0.000 -0.012 -0.812	MZ (kNm) 9.313 -0.001 2.996 2.936 0.042 0.042 0.042 10.585 1.280 -1.080 0.025				
Node 1	tions 1/8X 2/9Z 3/9X 4/97 4/97 4/97 4/97 4/97 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 7/FL 20/04 20	FX (kN) -3.007 0.000 1.206 -1.192 -0.077 0.004 0.583 -0.070 -4.286 -1.270 0.550	FY (kN) 366.143 -0.019 -0.836 0.832 186.848 5.758 918.427 168.192 24.375 -24.359 -0.002	FZ (kN) 0.000 -5.571 -0.000 -0.000 -0.000 -0.000 -0.000 8.356 -1.270 -4.286 0.521	(kNm) 0.001 -11.858 -0.000 0.000 -0.000 -0.004 -0.004 17.786 -1.259 -10.583 1.005	MY (kNm) 0.001 0.012 0.000 0.000 -0.000 -0.000 -0.000 -0.004 -0.018 -0.000 -0.000 -0.000 -0.000 -0.000	MZ (kNm) 9.313 -0.001 -2.906 0.046 -0.065 -0.652 0.042 10.685 1.280 -1.059				
Node 1	LIG 1.5X 2.52 3.5X 4.5X 4.5X 2.52 3.5X 4.5X 2.5Z 2.5Z 2.5Z 2.5Z 3.5X 4.5X 2.5Z 3.5X 4.5X 5.0L 5	FX (kN) -3.007 0.000 1.206 -1.192 -0.077 0.004 0.583 -0.070 -4.286 -1.270 0.530 -0.521 -0.521 -0.171	FY (kN) 366.143 -0.019 0.836 0.832 186.848 5.758 918.427 168.192 244.375 -24.359 0.002 0.002 142.575	FZ (kN) 0.000 -5.571 -0.0000 -0.000	(kNm) 0.001 -11.858 -0.000 0.000 -0.000 -0.000 -0.000 -1.259 -10.583 1.025 -1.050 0.190	MY (kNm) 0.001 0.012 0.000 0.000 -0.000 -0.004 -0.018 -0.000 -0.018 -0.000 -0.000 -0.000 -0.812 -0.812 0.001	M2 (kNm) 9.313 -0.001 -2.966 0.005 -0.102 0.042 10.688 1.260 -1.020 -1.020 -1.020				
Node 1	tions 1/5X 2/52 3/32	FX (kN) -3.007 0.000 1.206 -1.192 -0.077 0.004 0.583 -0.077 -0.070 -4.286 -1.270 0.530 -0.530 -0.521 -0.171 -0.003	FY (kN) 36.143 -0.019 -0.836 0.836 5.758 918.427 168.192 24.375 -24.359 0.002 0.002 0.002 142.575 3.706	FZ (kN) 0.000 -5.571 -0.0000 -0.00000 -0.0000 -0.0000 -0.0000 -0.0000 -0.0000 -0.00000 -0.000	(kNm) 0.001 -11.858 -0.000 0.000 -0.001 -0.001 -0.004 17.786 -1.259 -10.883 1.025 -1.050 0.190 0.004	MY (kNm) 0.001 0.012 0.000 0.000 0.000 0.000 0.000 0.000 0.018 0.000 0.018 0.000 0.018 0.000 0.018 0.000 0.012 0.001 0.000	MZ (kNm) 9.313 -0.001 2.2966 2.030 0.046 -0.065 10.046 10.046 10.046 10.046 10.046 10.046 10.046 10.046 0.048 0.048 0.048 0.058 0.004				
Node 1	LIC 1.8X 2.92 3.WX 4.WZ 5.0L 6.0L 2.5Z 2.5Z 3.WX 4.WZ 2.5Z 3.WX 4.WZ 0.L 7.FL	FX (kN) -3.007 -0.000 -1.206 -1.192 -0.077 -0.004 -0.583 -0.070 -4.286 -1.270 -0.530 -0.521 -0.171 -0.0353	PY (kN) 36.143 -0.019 -0.836 0.836 0.836 0.836 5.758 0.18.427 168.192 24.375 -24.359 0.002 0.0000 0.002 0.00000000	FZ (kN) 0.0000 0.0000 0.0000 0.0000 0.000000	(kNm) 0.001 -11.858 -0.000 0.000 -0.001 -0.000 -0.000 17.786 -1.259 -10.853 1.025 -1.050 0.190 0.004 0.629	MY (kNm) 0.001 0.002 0.000 0.000 0.000 -0.000 -0.004 -0.004 -0.000 -0.000 -0.004 -0.001 -0.000 -0.001 -0.000 -0.001 -0.000 -0.001 -0.000 -0.001 -0.001 -0.001 -0.001 -0.001 -0.001	MZ (kNm) 9.313 -0.001 -2.966 2.930 0.046 -0.005 -0.046 1.260 -1.058 1.260 -1.058 1.260 -1.0588 -1.0588 -1.0588 -1.0588 -1.0588 -1.0588 -1.0588 -1.0588 -1.0588 -1.0588 -1.0588 -1.0588 -1.0588 -1.0588 -1.0588 -1.05				

7) Reactions

\sim	CIRCULA	R WAT	ER T	ANK		Job No			553	Rev
						Part			100000	
36	oftware licensed to					Ref				
-										
						By		Det+30-N		
						File wate	er tank1.std		Date/Time 11-N	lay-2022
Reac	tions Con									
		Horizontal	Vertical	Horizontal		Moment				
Node	L/C	FX	FY	FZ	MX (kNm)	(kNm)	MZ			
		(kN)	(kN)	(kN)			(kNm)			
	3:WX	0.000	0.833	1.192	2.930	0.000	-0.000			
	4:WZ	-0.000	186,752	0.078	0.049	0.001	-0.001			
	6:LL	0.000	5.754	-0.004	-0.005	0.000	-0.001			
	7:FL	-0.109	633 297	-0.382	-0.526	-0.059	0.800			
	28:GENERATE	0.000	222.263	4.582	14.013	0.001	-0.001			
4	1:SX	-4,286	-24.397	1.270	1.259	-0.001	10.585			
-	2:SZ	1,271	-24.400	-4.286	-10.583	0.000	-1.260			
	3:WX	-0.530	0.001	0.521	1.025	-0.812	1.050			
	4:WZ	0.521	0.003	-0.530	-1.050	0.812	-1.025			
	5:DL	0.171	142.753	0.171	0.192	-0.000	-0.191			
	6:LL	0.003	3.714	0.003	0.004	-0.000	-0.004			
	7:FL	0.268	283,907	0.152	0.198	0.043	0.348			
	28:GENERATE	-1.752	165.078	6.583	16.048	-0.001	1.717			
5	1:SX	-3.007	-36,145	-0.000	-0.001	0.001	9.314			
	2:87	-0.000	0.004	-5.571	-11.858	-0.012	0.001			
	3:WX	-1.206	-0.833	0.000	0.000	-0.000	2.966			
	4:WZ	1.102	0.820	-0.000	-0.000	0.000	-2.030			
	5:DL	0.078	186.614	0.000	0.001	-0.001	-0.048			
	6:LL	-0.004	5.748	0.000	0.000	-0.000	0.005			
	7:FL	-0.186	347.968	0.002	0.005	-0.004	0.911			
	28:GENERATE	0.071	167.947	8.356	17.788	0.017	-0.044			
6	1:SX	-4.286	-24.340	-1.271	-1.261	0.001	10.583			
	2:SZ	-1.271	24.396	-4.286	-10.584	0.001	1.260			
	3:WX	-0.530	-0.002	-0.521	-1.025	0.812	1.050			
	4:WZ	0.521	0.006	0.530	1.050	-0.812	-1.025			
	5:DL	0.170	142.760	-0.171	-0.189	0.000	-0.188			
	6:LL	0.003	3.714	-0.003	-0.004	0.000	-0.004			
	7:FL	0.265	283.842	-0.149	-0.185	-0.042	0.361			
-	28:GENERATE	2.060	91.890	6.275	15.706	-0.001	-2.060			
7	1:SX	-5.571	-0.014	-0.000	-0.000	-0.013	11.858			
	2:8Z	-0.000	36.116	-3.008	-9.314	0.000	0.000			
	3:WX	-0.000	0.836	-1.192	-2.930	0.000	0.000			
	4:WZ	0.000	-0.840	1.205	2.966	-0.000	-0.000			
	5:DL	-0.001	186.725	-0.079	-0.049	0.001	0.001			
	6:LL	-0.000	5.752		0.005	0.000	0.000			
	7:FL	-0.112	633.170	0.382	0.525	0.067	0.809			
0	28:GENERATE	-0.001	113.878	4.441	13.927	0.001	0.001			
8	1:SX	-4.285	24.361	1.271	1.261		10.583			
	2:SZ 3:WX	1.271	24.386	-4.286	-10.584	-0.001	-1.260			
	3:WX 4:WZ	0.530	0.000	-0.521	-1.025	-0.812	-1.050			
	4:W2 5:DL	-0.521	142.606	-0.172	-0.193	-0.001	0,191			
	6:LL	-0.171	3,708	-0.172	-0.193	-0.001	0.191			



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XII. CONCLUSION

It concludes that the efficiency and reliability of the software in the field of designing is much better to that of them annual work. It has been seen that these off ware generated results were more efficient and economical which included the various different conditions under the designing conditions which are difficult to consider when done manually

- 1) The structural elements of water tank are safe in leakage free, flexure and shear.
- 2) Quantity of steel provided for structure is economical and adequate.
- 3) Proposed sizes of structural elements can be used in water tank as it is.
- 4) The design of beam, slab, column, footing and stair case are out of danger in deflection, bending, shear and other aspects.

Water tanks are considered to be effusive; but they are constructed to reach present and coming time population. They are considered to highly unreasonable and safely store the portable water. Water can be distributed to number of homes, Industries and public places which means of a network of a water distribution system. Hence water tanks are considered to be supporting systems and useful for the community. In circular tanks, as height increases as side wall thickness are to be increases and roof slab and floor slab depth are decreases. The circular water tanks are economical for average capacities. Design of water tank is a very irksome method. Particularly design of underground water tanks are lots of mathematical formulae and calculation. It is also more time consuming.

XIII. SCOPE OF FURTHERWORK

Design of water tank is a very difficult method. It uses for lots of mathematical calculation & uses of formulas for unusually design of overhead water tank. It is to be time consuming method. Thus works arte gives a solution to the above problems. There is a small difference between the design values of works to that of manual calculation. This works gives the least value for the design. Thus the designer should not provide less than the values we get from the works. In case of theoretical calculation designer initially added some extra values to the obtained values tobe the safer side.

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