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International Journal For Research in  
Applied Science and Engineering Technology



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# INTERNATIONAL JOURNAL FOR RESEARCH

IN APPLIED SCIENCE & ENGINEERING TECHNOLOGY

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**Volume:** 12    **Issue:** XI    **Month of publication:** November 2024

**DOI:** <https://doi.org/10.22214/ijraset.2024.65071>

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# Modeling of Microstrip line Gap Discontinuity on Multilayer Substrate

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**Abstract:** In this paper, the modeling of microstrip line gap discontinuity on multilayer semiconductor substrate is presented. The reflection coefficient and transmission coefficient are computed from the equivalent lumped circuit model of microstrip line gap discontinuity. The lumped circuit elements- capacitance, inductance and resistance are calculated using closed-form expressions in term of the gap discontinuity, width of microstrip line and dielectric substrate thickness. Static Spectral Domain Analysis (SDA) method is used to compute characteristic impedance of microstrip line.

**Keywords:** Static Spectral Domain Analysis, Gap Discontinuity, Multilayer Microstrip line.

## I. INTRODUCTION

Microstrip line are used in the design of microwave integrated circuits (MICs) and monolithic MICs. The microwave components such as couplers, filters, interconnecting lines and matching components are essential part of a complex microwave circuits in hybrid and monolithic MICs. Discontinuities such as open-end, step and gap discontinuity are widely used in the microwave components design. For frequency dependent analysis, Full wave methods have been used, but these methods are complex and difficult to implement. Circuit model provides fast and accurate results at low frequencies; hence circuit models are used at low frequency for circuit design. [1-9]. The circuit model for gap discontinuity has been modified by incorporating lumped circuit elements. The results are compared with full-wave spectral domain analysis [5].

For the hybrid and semiconductor based integrated circuits, it is important to analyze and characterize the microstrip line discontinuities on multilayer substrate. This paper presents analysis of microstrip line gap discontinuity on multilayer substrate. For this, the static spectral domain analysis method and single layer reduction (SLR) technique are used to obtain the effective relative permittivity and characteristic impedance of microstrip line. The equivalent circuit model has been used to compute the frequency dependent reflection coefficient and transmission coefficient of microstrip line gap discontinuity. In section-II, SDA method for multilayer microstrip line is discussed. The circuit model for gap discontinuity and calculated numerical results are discussed in section-III and Section-IV respectively.

## II. ANALYSIS OF MULTILAYER MICROSTRIP LINE

In this paper, Galerkin's technique based static SDA method have been used for computing the capacitance of multilayer microstrip line. The characteristic impedance is computed from the line capacitance. The Green's function in Fourier domain for multilayer microstrip line structure is obtained using transverse transmission line (TTL) technique [10-12].

The cross section of a shielded multilayer microstrip line is shown in Fig.1. The width of strip is S. The thickness of lower and upper dielectric substrate is H<sub>1</sub> and H<sub>2</sub> respectively. The permittivity of dielectric substrate is ε<sub>1</sub> and ε<sub>2</sub>. The capacitance is computed from following relation [10-12].

$$\frac{1}{C} = \frac{L}{2\epsilon_0 Q^2} \sum_{n=1}^{\infty} \tilde{\rho}_s^2(\beta_n, y) \tilde{G}(\beta_n, y) \quad (1)$$

where  $\tilde{G}(\beta_n, y)$  is Fourier transform of Green's function,  $\tilde{\rho}_s$  is Fourier transform of charge distribution and Q is total charge present on strip. The characteristic impedance is computed from Equation (2).

$$Z_o = \frac{1}{c\sqrt{C_d C_{air}}} \quad (2)$$

where c is velocity of light in free space, C<sub>d</sub> is capacitance with dielectric substrate, and C<sub>air</sub> is capacitance when dielectric is replaced with air.

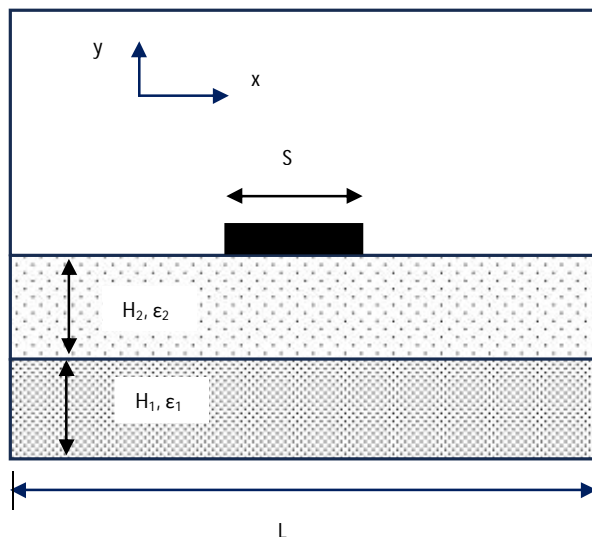


Fig.1 Multilayer Microstrip Line

### III. MICROSTRIP LINE GAP DISCONTINUITY

The microstrip line gap discontinuity and its equivalent circuit model are shown in Fig.2(a) and Fig.2(b) respectively. This circuit model pi-network of admittance parameters. The closed form expression for capacitance, inductance and resistance are calculated in terms of physical parameters of microstrip line, i.e., width of strip conductor (S), gap (G) and thickness of dielectric substrate [5].

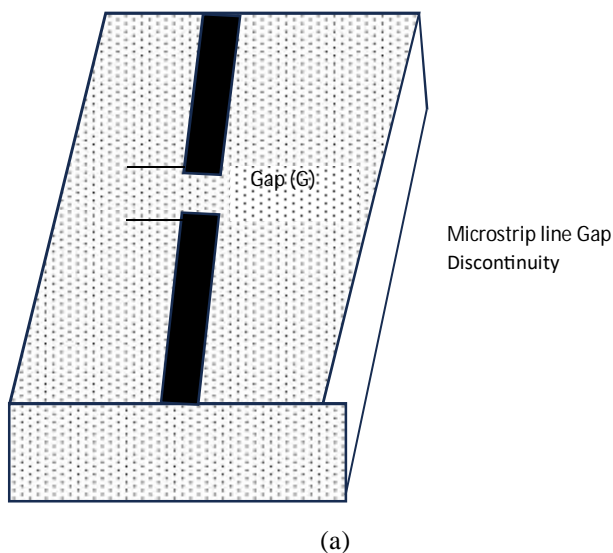
$$C_{11} = \left(\frac{1}{Z_0}\right) (A1) \cdot \tanh(A2) \text{ pF} \tag{3(a)}$$

$$A1 = 1.125 \tanh\left(\frac{1.358S}{H_t}\right) - 0.315$$

$$A2 = \left(0.0262 + 0.184 \frac{H_t}{S}\right) + \left(0.217 + 0.0619 \ln\left(\frac{S}{H_t}\right)\right) \frac{G}{H_t}$$

$$C_{12} = \left(\frac{1}{Z_0}\right) (B1) \cdot \tanh(B2) \text{ pF} \tag{3(b)}$$

$$B1 = 6.832 \tanh\left(\frac{0.0109S}{H_t}\right) + 0.91, \quad B2 = \left(1.411 + 0.314 \frac{H_t}{S}\right) + \left(\frac{G}{H_t}\right)^{1.248 + 0.36 \tan^{-1} \frac{S}{H_t}}$$



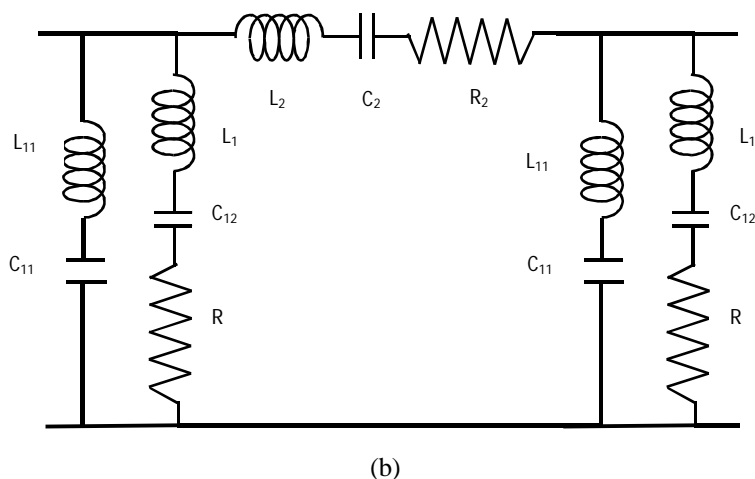


Fig.2 Microstrip line (a) Gap Discontinuity and (b) Equivalent Circuit Model

$$L_{11} = (Z_o)D1 * exp(D2) \text{ nH} \tag{3(c)}$$

$$D1 = 0.134 + 0.0436 \ln\left(\frac{H_t}{S}\right), \quad D2 = -\left(3.656 + 0.246 \frac{H_t}{S}\right) \cdot \left(\frac{G}{H_t}\right)^{1.739+0.39 \ln \frac{S}{H_t}}$$

$$L_{12} = (Z_o) \left( E1 + \left(0.1827 + 0.00715 \ln \frac{S}{H_t}\right) * exp(E2) \right) \text{ nH} \tag{3(d)}$$

$$E1 = 0.008285 \tanh\left(\frac{0.5665S}{H_t}\right) + 0.0103$$

$$E2 = -\left(5.207 + 1.283 \tanh\left(\frac{1.656H_t}{S}\right)\right) \cdot \left(\frac{G}{H_t}\right)^{0.542+0.873 \tan^{-1} \frac{S}{H_t}}$$

$$R_1 = (Z_o) \cdot F1 * \tanh(F2) \text{ ohm} \tag{3(e)}$$

$$F1 = 1.024 \tanh\left(\frac{2.025S}{H_t}\right), \quad F2 = \left(0.01584 + 0.0187 \frac{H_t}{S}\right) \frac{G}{H_t} + 0.1246 + 0.0394 \sinh\left(\frac{S}{H_t}\right)$$

$$C_2 = J1 + (J2) \cdot \text{sech}\left(\frac{2.3345G}{H_t}\right) \text{ pF} \tag{3(f)}$$

$$J1 = \left(0.1776 + 0.05104 \ln \frac{S}{H_t}\right) \frac{H_t}{G}, \quad J2 = \left(0.574 + 0.3615 \frac{H_t}{S} + 1.156 \ln\left(\frac{S}{H_t}\right)\right)$$

$$L_2 = (Z_o)(K1) \cdot \sinh\left(\frac{2.3345G}{H_t}\right) \text{ nH} \tag{3(g)}$$

$$K1 = \left(0.00228 + \frac{0.873}{7.52 \left(\frac{S}{H_t}\right) + \cosh\left(\frac{S}{H_t}\right)}\right)$$

$$R_2 = (Z_o) \left( M1 + (M2) \cdot \sinh \frac{2.3345G}{H_t} \right) \text{ ohm} \tag{3(h)}$$

$$M1 = \left(-1.78 + \frac{0.749S}{H_t}\right) \frac{G}{H_t}, \quad M2 = \left(1.196 - 0.971 \ln\left(\frac{S}{H_t}\right)\right)$$

$$H_t = H_1 + H_2$$

The admittance parameters of circuit is evaluated from the lumped parameters of equivalent circuit using Equation 3(a)-3(h). From the admittance parameters equivalent circuit, the frequency dependent reflection coefficient and transmission coefficient are computed [5].

#### IV. NUMERICAL RESULT AND DISCUSSION

Microstrip line gap discontinuity is present on two-layer dielectric substrates. First layer is silicon (Si) dielectric substrate  $\epsilon_{r1} = 11.9$  and thickness  $H_1 = 0.4\text{mm}$ . Above the silicon dielectric substrate, a thin silicon dioxide layer is present. The relative permittivity of silicon dioxide is  $\epsilon_{r2} = 3.9$  and thickness  $H_2 = 3\mu\text{m}$ . The width of microstrip line strip is  $S=0.3\text{mm}$ . The characteristic impedance for  $S=0.3\text{mm}$  is  $52.6\text{ ohm}$ . For different gap ( $G$ ) ranging from  $10\mu\text{m}$  to  $20\mu\text{m}$ ,  $30\mu\text{m}$  and  $40\mu\text{m}$ , the lumped circuit parameters are calculated.

Fig. 3(a) and Fig. 3(b) shows the variation of reflection coefficient (mag.) and reflection coefficient (phase, deg.) with frequency for different gap ( $G$ ) discontinuity. More field is radiated from the edges of gap discontinuity with increase of frequency. Due to increase of frequency, radiation loss and surface wave loss increases. For  $G=10\mu\text{m}$  and  $G=40\mu\text{m}$ , reflection coefficients are  $0.34$  and  $0.62$  respectively at  $30\text{GHz}$ . Furthermore, the magnitude and phase angle of transmission coefficient are also plotted in Fig. 4(a) and Fig. 4(b) respectively for four gap,  $G=10\mu\text{m}$ ,  $20\mu\text{m}$ ,  $30\mu\text{m}$  and  $40\mu\text{m}$ . As frequency increases, the radiation loss and surface wave loss increases. The higher order modes are also generated at high frequencies. Therefore, as the operating frequency increases, the transmission coefficient also increases.

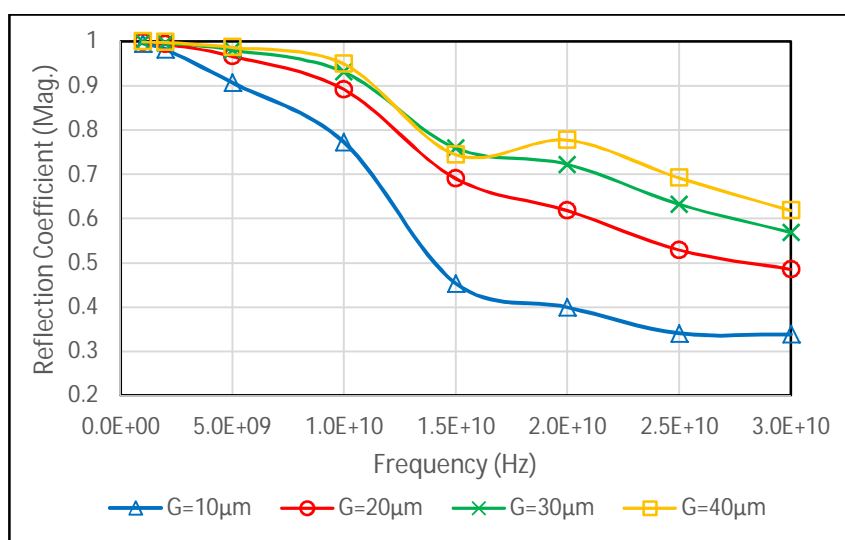


Fig. 3(a) Reflection Coefficient (Mag.)

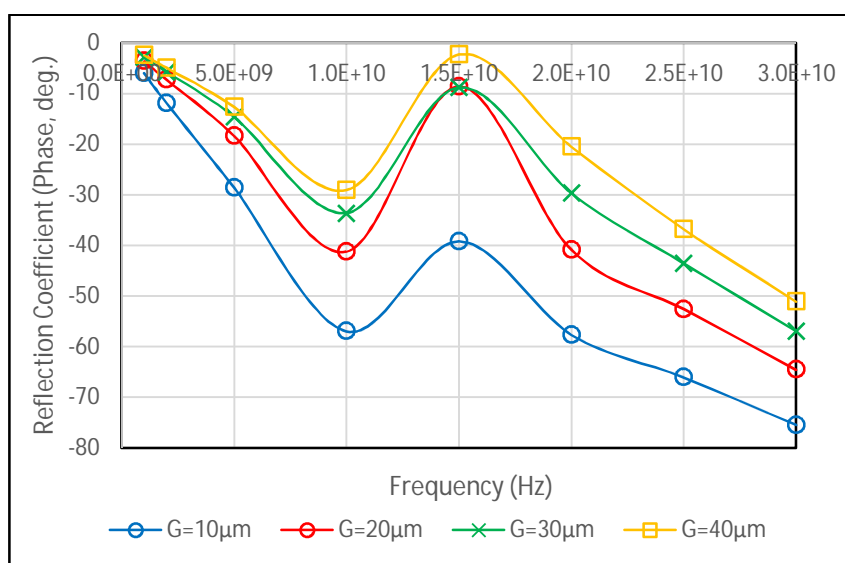


Fig. 3(b) Reflection Coefficient (Phase, deg.)

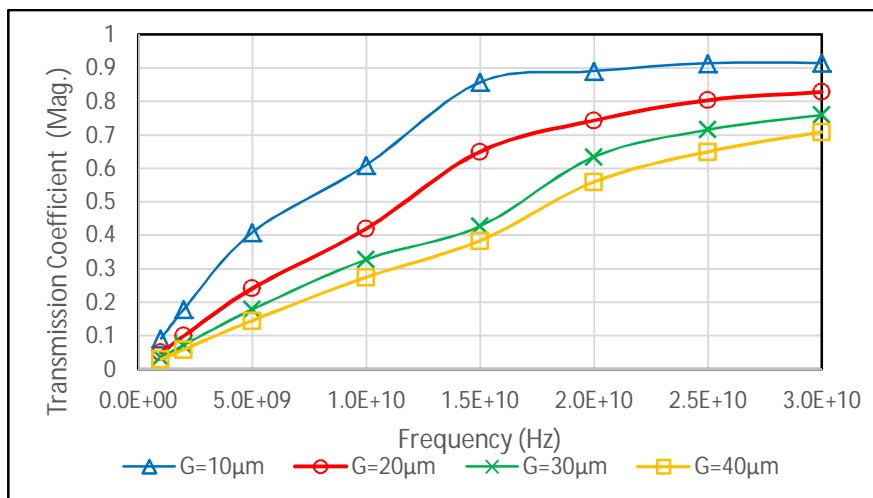


Fig. 4(a) Transmission Coefficient (Mag.)

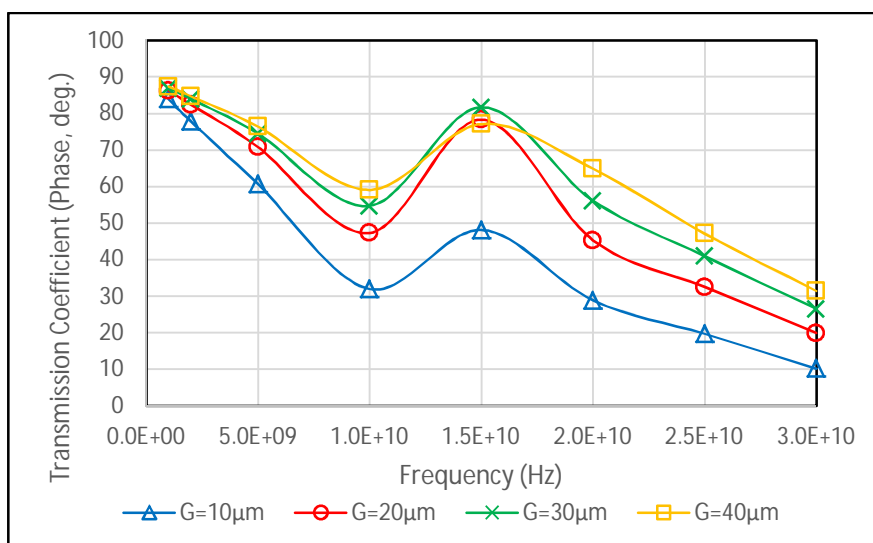


Fig. 4(b) Transmission Coefficient (Phase, deg.)

## V. CONCLUSION

In this paper, equivalent lumped circuit model of microstrip line gap discontinuity on multilayer semiconductor substrate has been analyzed. The circuit model can be used to study and compute the reflection and transmission coefficient of gap discontinuity on multilayer substrate.

## REFERENCES

- [1] Nikolaos K. Uzunoglu, Christos N. Capsalis and Constantinos P. Chronopoulos, Frequency-Dependent Analysis of a Shielded Microstrip Step Discontinuity Using an Efficient Mode Matching Technique, IEEE Transactions on Microwave Theory and Techniques, Vol. 36, No. 6, June 1988, pp. 976-984.
- [2] HungYu Yang, Nicolaos G. Alexopoulos and David R. Jackson, Microstrip Open-End and Gap Discontinuities in a Substrate-Superstrate Structure, IEEE Transactions on Microwave Theory and Techniques, Vol. 37, No. 10, October 1989 pp. 1542-1546.
- [3] W. Tang, Y. L. Chow and K. F. Tsang, Different microstrip line discontinuities on a single field- based equivalent circuit model, IEE Proc.-Microwave, Antenna Propagation, Vol. 151, No. 3, June 2004, pp. 256-262.
- [4] Raine N. Simons, Nihad I. Dib and Linda P. B. Katehi, Modeling of Coplanar Stripline Discontinuities, IEEE Transactions on Microwave Theory and Techniques, Vol. 44, No. 5, May 1996 pp. 711-716.
- [5] Nicolaos G. Alexopoulos and Shih-Chang Wu, Frequency-Independent Equivalent Circuit Model for Microstrip Open-End and Gap Discontinuities, IEEE Transactions on Microwave Theory and Techniques, Vol. 42, No. 7, July 1994, pp. 1268-1272.
- [6] Jaideva C. Goswami, Andrew K. Chan and Charles K. Chui, Spectral Domain Analysis of Single and Coupled Microstrip Open Discontinuities with Anisotropic Substrate, IEEE Transactions on Microwave Theory and Techniques, Vol. 44, No. 7, July 1996, pp. 1174-1178.



- [7] Jesus Martel, Rafael R. Boix and Manuel Horno, Static Analysis of Microstrip Discontinuities Using the Excess Charge Density in the Spectral Domain, IEEE Transactions on Microwave Theory and Techniques, Vol. 39, No. 9, September 1991, pp. 1623-1631.
- [8] William J. Getsinger, End-Effects in Quasi-TEM Transmission Lines, IEEE Transactions on Microwave Theory and Techniques, Vol. 41, No. 4, April 1993, pp. 666-672.
- [9] Guoan Wang, Hanyi Ding, Amit Bavisi, Kwanhim Lam and Essam Mina, On-Chip 3-D Model for Millimeter-Wave T-Lines with Gap Discontinuity in BiCMOS Technology, Proceedings of Asia-Pacific Microwave Conference 2007.
- [10] Cam Nguyen, Analysis Methods for RF, Microwave, and Millimeter-Wave Planar Transmission Line Structures, John Wiley & Sons, Inc., 2000.
- [11] Anand K. Verma, Paramjeet Singh and Ladislau Matekovits, Strip-Width and Slot-Gap Dependent Equivalent Isotropic Substrate and Dispersion Characteristics of Asymmetric Coplanar Waveguide, Symmetric Coplanar Waveguide and Micro-Coplanar Strip Line on Anisotropic Substrates, IEEE Transactions on Microwave Theory and Techniques, Vol. 62, No. 10, October 2014, pp. 2232-2241.
- [12] A. K. Verma, Paramjeet Singh and Ritu Bansal, Computation of Static and Frequency-Dependent Line Parameters of Multilayer CPW Using Static SDA and Single Layer Reduction Method, International Journal of RF and Microwave Computer-Aided Engineering, Vol. 24, No. 1, January 2014, pp. 18-29.



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