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# An Effective Design of Speed Controller for Permanent Magnet Synchronous Motor Using Fuzzy Technique

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**Abstract:** A permanent magnet synchronous motor (PMSM) features low inertia, high power density, low noise, high efficiency, low maintenance cost, and robustness, a PMSM has been widely used in many industrial applications. However, precise control of a PMSM is not easy due to nonlinearities of PMSM servo systems, parameter and load torque variations. Thus the linear control schemes such as PI control cannot guarantee satisfactory performances. In this paper a Simulink model of PMSM is derived from mathematical model. Then fuzzy model of PMSM is developed based on Takagi–Sugeno fuzzy approach, also a fuzzy speed regulator based on the Takagi–Sugeno fuzzy approach is designed for a PMSM. Simulation results are given to verify that the proposed method can be successfully used to control a PMSM under parameter and load torque variations.

**Keywords:** Fuzzy system, (PMSM), speed control, Takagi–Sugeno fuzzy model .

## I. INTRODUCTION

A Permanent Magnet Synchronous Motor (PMSM) has low inertia, high power density, low noise, high efficiency, low maintenance cost, high torque density, and robustness. The permanent magnet synchronous motor eliminates the use of slip rings for field excitation, resulting in low maintenance and low losses in the rotor. Thus, a PMSM has been widely used in many industrial applications such as chip mount machines, semiconductor production machines, high-resolution computer-numerical-control machines, robots, and hard disk drives. But, precise control of a PMSM is not easy due to the nonlinearities of PMSM servo systems, parameter variations, and load torque variations. The main drawbacks of the linear control approach are the sensitivity in performance to the system parameters variations and inadequate rejection of external perturbations and load changes. Thus, the linear control schemes such as proportional–integral control cannot assure satisfactory performances. To remove this problem, many researchers have proposed various control design methods. e.g., neural network control [2], adaptive control [3][5], and disturbance-observer-based control. Fuzzy-logic, first proposed by L. A. Zadeh, has recently received a great deal of attention. The easy way of

defining a fuzzy controller by rules with an obvious physical meaning has helped to expand this control technique. When it is applied to control nonlinear systems, this nonlinear control strategy has shown better results than classical controllers do.

## II. PMSM MODEL

By taking the rotor coordinates of the motor as reference coordinates, a surface-mounted PMSM can be represented by the following nonlinear equation

$$V_{qs}^r = (r_s + pL_q)i_{qs}^r + \omega_r L_d i_{ds}^r + \omega_r \lambda_m^r \quad (1)$$

$$V_{ds}^r = (r_s + pL_d)i_{ds}^r - \omega_r L_q i_{qs}^r \quad (2)$$

$$T_e = \frac{3}{2} \left( \frac{P}{2} \right) (\lambda_m^r i_{qs}^r + (L_d - L_q) i_{qs}^r i_{ds}^r) \quad (3)$$

$$T_e = T_L + B\omega_m + J \cdot p\omega_m \quad (4)$$

Where

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$$\omega_m = \omega_r \left(\frac{p}{2}\right)$$

P denotes no. of poll and p differentiation.

By using equation 1 through 4, a surface-mounted PMSM can be represented by the following nonlinear equation

$$\omega_r^* = k_1 i_{qs}^r - k_2 \omega_r - k_3 T_L \tag{5}$$

$$i_{qs}^{r*} = -k_4 i_{qs}^r - k_5 \omega_r + k_6 V_{qs} - \omega_r i_{ds}^r \tag{6}$$

$$i_{ds}^{r*} = -k_4 i_{ds}^r + k_6 V_{ds} + \omega_r i_{qs}^r \tag{7}$$

Where \* denotes differentiation  $T_L$  represents the load torque,  $\omega_r$  is the electrical rotor angular speed, and  $k_i > 0, i = 1 \dots 6$ , are the parameter values given by  $k_1 = \frac{3}{2} \frac{1}{J} \frac{p^2}{4} \lambda_m, k_2 = \frac{B}{J}, k_3 =$

$$\frac{p}{2J}, k_4 = \frac{R_s}{L_s}$$

$$k_5 = \frac{\lambda_m}{L_s}, k_6 = \frac{1}{L_s}$$

We want to design a T-S control system so a T-S model of PMSM is required. In T-S fuzzy modeling n operating points for a nonlinear system are first chosen, then a set of n simple local linear subsystem models for each operating point is obtained, and each subsystem model is associated with a fuzzy inference rule. Based on the T-S fuzzy modeling approach, the PMSM model can be approximated by a third order r-rule fuzzy model. The  $i^{th}$  rule of the T-S fuzzy model is of the following form

Plant Rule i : If  $i_s$  is  $F_i$ , Then

$$\omega_r^* = k_1 i_{qs}^r - k_2 \omega_r - k_3 T_L$$

$$i_{qs}^{r*} = -k_4 i_{qs}^r - k_5 \omega_r + k_6 V_{qs} - \omega_r i_{ds}^r$$

$$i_{ds}^{r*} = -k_4 i_{ds}^r + k_6 V_{ds} + \omega_r i_{qs}^r$$

where  $F_i (i = 1, \dots, n)$  values denote the fuzzy sets,  $n$  is the number of fuzzy rule,  $(I_{qsi}, I_{dsi})$  is the  $i^{th}$  operating point, and  $i_s = [i_{qs}, i_{ds}]^T$ . Each fuzzy set  $F_i$  is characterized by a membership function  $m_i(i_s)$  and the  $i^{th}$  operating point  $(i_{qs}, i_{ds}) = (I_{qsi}, I_{dsi})$ . By using a standard T-S fuzzy inference mechanism, the following global nonlinear model of PMSM can be obtained

$$\omega_r^* = k_1 i_{qs}^r - k_2 \omega_r - k_3 T_L \tag{8}$$

$$i_{qs}^{r*} = -k_4 i_{qs}^r - k_5 \omega_r + k_6 V_{qs} - \sum_{i=1}^n h_i(i_s) I_{dsi}^r \omega_r \tag{9}$$

$$i_{ds}^{r*} = -k_4 i_{ds}^r + k_6 V_{ds} + \sum_{i=1}^n h_i(i_s) I_{qsi}^r \omega_r \tag{10}$$

where  $h_i(\cdot) = m_i(\cdot) / \sum_{j=1}^n m_j(\cdot), m_i: R^2 \rightarrow [0, 1], i = 1, \dots, n$  is the membership function of the system with respect to plant rule  $i, h_i$  can be regarded as the normalized weight of each if-then rule and satisfies  $m_i(i_s) \geq 0$  and  $\sum_{i=1}^n m_i(\cdot) = 1$

Assuming two operating point such that  $I_{qsi} = I_{qs2} = I_0, I_{ds1} = -I_{ds2} = I_0$  and  $m_i(i_s)$  are given by

$$m_1 = \frac{e^{-\mu(i_{ds}^r - I_0)^2}}{e^{-\mu(i_{ds}^r - I_0)^2} + e^{-\mu(i_{ds}^r + I_0)^2}}$$

$$m_2 = 1 - m_1$$

Simulink model for fuzzy PMSM model is made of various subsystems these subsystem model are given here

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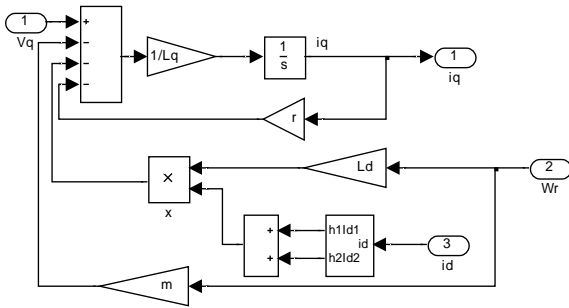


Figure 1: q-axis T-S fuzzy model

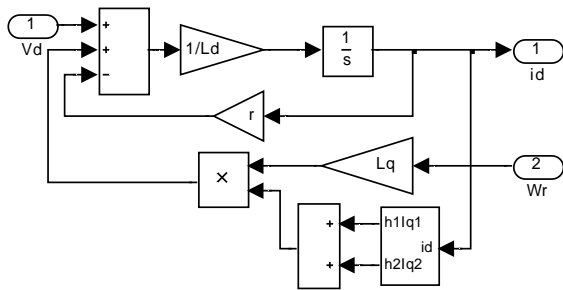


Figure 2: d-axis T-S fuzzy model

These blocks are combined along with abc to d-q conversion block, to get complete fuzzy model of Permanent magnet synchronous motor.

III. FUZZY SPEED REGULATOR DESIGN

Let us define  $i_{qsd}$  as  $i_{qsd} = (k_2\omega_d + k_3T_L)/k_1$ , then by using assumptions that  $v_a$  'T<sub>L</sub>\* is unknown and T<sub>L</sub>\* can be neglected, and it can be set as T<sub>L</sub>\* = 0', and the desired speed  $\omega_d$  is constant and  $\omega_d^* = 0$ , it can be shown that  $i_{qsd}^* = 0$ . Taking  $\tilde{\omega}$  and  $\tilde{i}_{qs}$  as  $\tilde{\omega} = \omega_r - \omega_d$  and  $\tilde{i}_{qs} = i_{qs}^r - i_{qsd}$  respectively.

Let the control input variables  $V_{qs}$  and  $V_{ds}$  be decomposed as

$$V_{qs} = \frac{1}{k_6}(u_q + u_{qf}), \quad V_{ds} = \frac{1}{k_6}(u_d + u_{df})$$

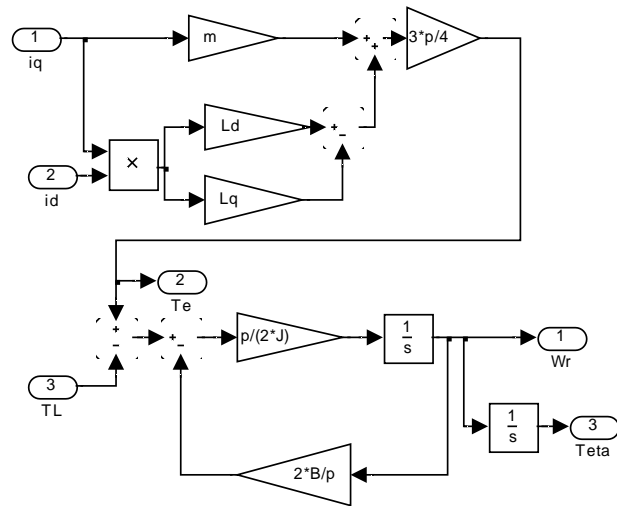


Figure 3: Torque and speed model

Then, fuzzy model can be transformed into

$$\tilde{\omega}^* = k_1\tilde{i}_{qs} - k_2\tilde{\omega}$$

$$\tilde{i}_{qs}^* = -k_4i_{qs}^r - k_5\omega_r + u_q + u_{qf} - \sum_{i=1}^n h_i(i_s)I_{dsi}^r \omega_r$$

$i_{ds}^{r*} = -k_4i_{ds}^r + u_q + u_{qf} + \sum_{i=1}^n h_i(i_s)I_{qsi}^r \omega_r$  Let the local speed regulator be given by the following linear controller

Controller Rule  $i$ : If  $i_s$  is  $F_i$ , then

$$u_q = k_4i_{qs}^r + (k_5 + I_{di})\omega_r$$

$$u_d = k_4i_{ds}^r - I_{qi}\omega_r$$

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$$u_{qdf} = k_i x$$

Where  $X = [\tilde{\omega}, \tilde{i}_{qs}, \tilde{i}_{ds}]^T$   $u_{qdf} = [u_{qf} \ u_{df}]^T$ , and  $K_i \in R^{2 \times 3}$  are gain matrices. Then, the final fuzzy speed regulator inferred as the weighted average of the each local controller is given by

$$u_q = k_4 i_{qs}^r + k_5 \omega_r + \sum_{i=1}^n h_i(i_s) I_{dsi}^r \omega_r \quad (11)$$

$$u_d = k_4 i_{ds}^r - \sum_{i=1}^n h_i(i_s) I_{qsi}^r \omega_r \quad (12)$$

$$u_{qdf} = \sum_{i=1}^n h_i(i_s) k_i x \quad (13)$$

Simulink model for fuzzy speed regulator is given in figure 4.

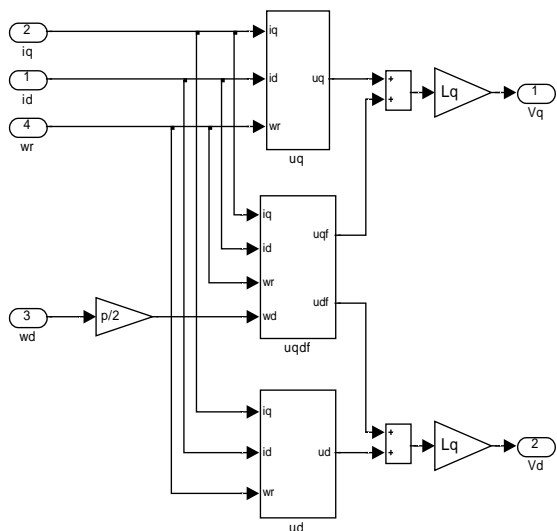


Figure 4: Simulink model of Fuzzy speed regulator

IV. SIMULATION RESULT

Table 1

Parameters	Rating
Rated phase voltage	230 V

Rated phase current	3.94 A
Number of poles (P)	12
Stator resistance(r)	0.99 Ω
Stator inductance(L <sub>d</sub> = L <sub>q</sub> )	5.82 mH
Magnetic flux(λ <sub>m</sub> )	0.079153 V.sec/rad
Equivalent inertia(J)	0.0012 kg.m <sup>2</sup>
Viscous friction coefficients(B)	0.0003 N.m.sec/rad

A PMSM given by equation 8, 9 and 10 is considered with nominal parameters values given in table 1, load torque is 1 N-m Two rule fuzzy model is assumed Two set point are given by  $I_{qs1} = I_{qs2} = I_0$ ,  $I_{ds1} = -I_{ds2} = I_0$ ,  $I_0 = 4$  and  $\mu = 0.0313$ . The controller gain matrix is given as

$$K_1 = 10^3 \times \begin{bmatrix} -0.2701 & -0.5271 & 0 \\ -0.0157 & 0 & -1 \end{bmatrix}$$

$$K_2 = 10^3 \times \begin{bmatrix} -0.0131 & -0.04232 & 0 \\ 0 & 0 & -1 \end{bmatrix}$$

Matlab/Simulink was used for simulation. Simulation was performed using fixed step of size 0.00001, Runge-Kutta method has been used for the solution of differential equations. For the simulation pulse-width modulation frequency is chosen as 45 kHz and space vector PWM (SVPWM) technique was used.

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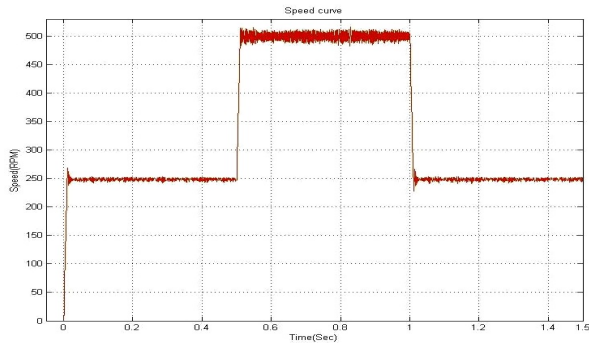


Figure 5: Motor speed with nominal parameters

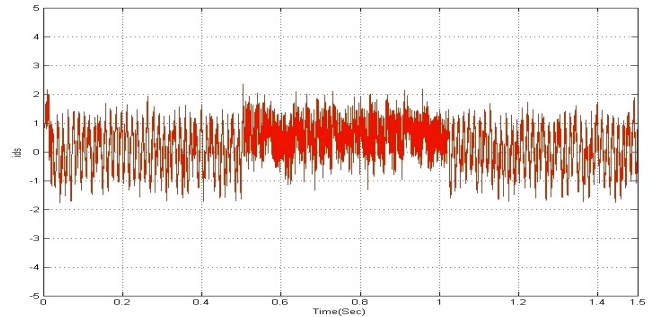


Figure 8:  $i_{ds}$  with nominal parameters

Firstly simulation with nominal parameters given in table 1 is performed. Figures 5 to 9 show the simulation results for the case when reference speed is increases from 250 rpm to 500 rpm and then decreases from 500 rpm to 250 rpm with nominal parameters.

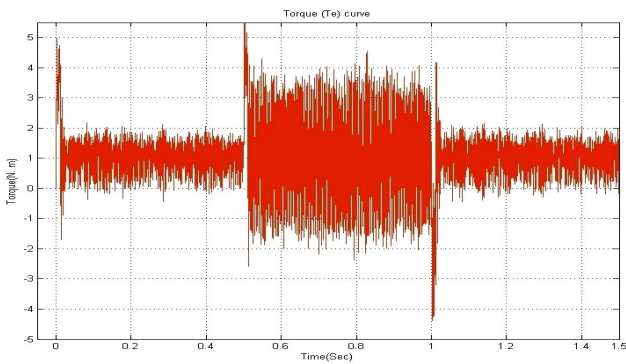


Figure 6: Electromagnetic torque with nominal parameters

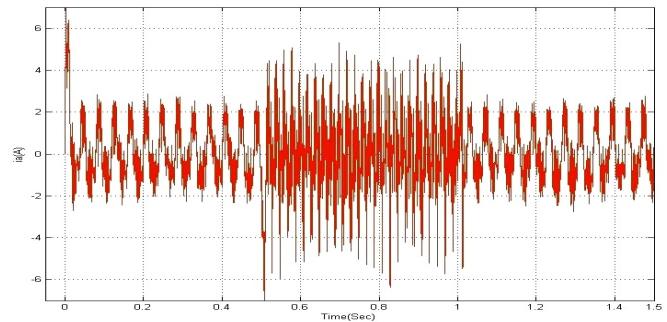


Figure 9:  $i_a$  with nominal parameters

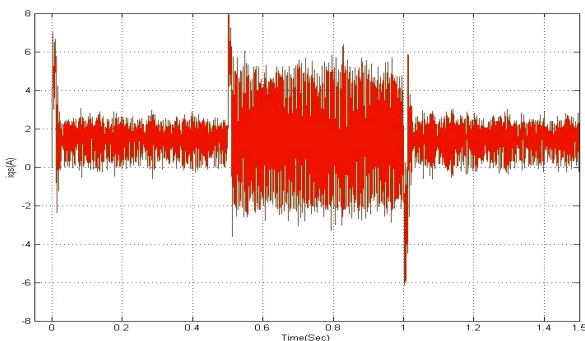
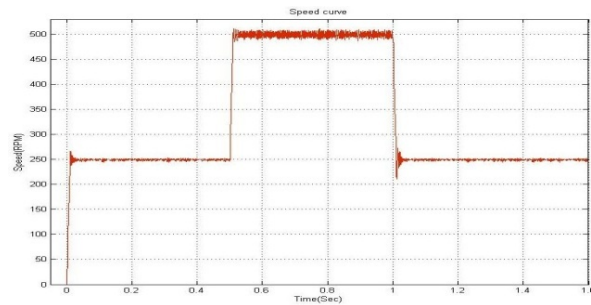


Figure 7:  $i_{qs}$  with nominal parameters

In second case simulation is performed with parameter variation of 125% of some parameter of table 1. The values of new parameters are  $r = 1.24 \Omega$ ,  $L_d = L_q = 7.28 \text{ mH}$ ,  $J = 0.0015 \text{ kg.m}^2$ ,  $T_L = 1.5 \text{ N.m}$ . The PMSM parameters usually vary due to aging, wear, and change of operating point. It can be verified that the proposed fuzzy controller gives very performance such as fast transient response, a small steady state error and a good performance under model parameter and load torque variation.



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Figure 10: Motor speed with parameter variation

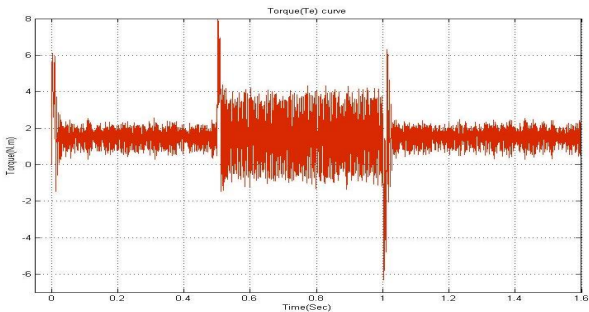


Figure 11: Electromagnetic torque with parameters variation

Figure 10 to 14 show the simulation result of the motor under parameter variation for same variation of speed as in case 1. Under these conditions also motor speed track the reference speed signal quit accurately.

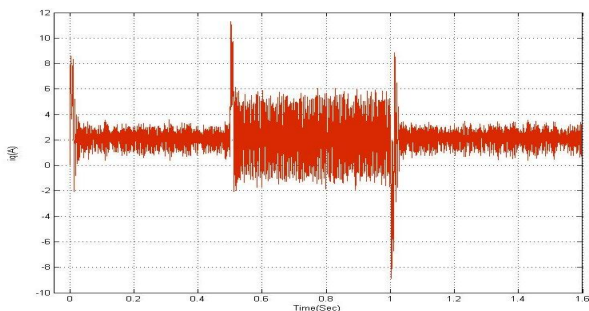


Figure 12 q-axis current with parameters variation

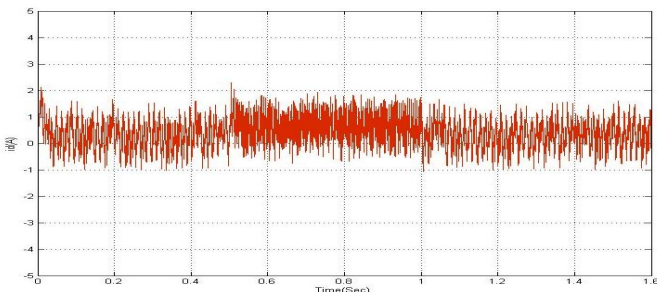


Figure 13: d-axis current with parameters variation

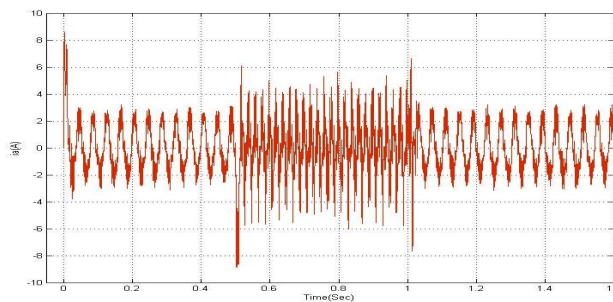


Figure 14: Motor phase current  $i_a$  with parameters variation

## CONCLUSION

Fuzzy model of PMSM is purposed and based on this fuzzy model T-S fuzzy speed regulator is given. In the last simulation for speed regulation was done using two rule T-S fuzzy model. Simulation is first time performed with nominal motor parameter and second time with 125% variation of some parameter. From the simulation results we conclude that the response of proposed fuzzy speed regulator is fast as compared to conventional speed controller. Effect of parameters variation on the performance of regulator is very low with fuzzy speed regulator. Performance is almost invariant with respect to parameters and load torque variations. Simulation results have been given to show the effectiveness of proposed design method.

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