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# **Design & Simulation of 6kW Wind Turbine**

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Abstract: In these ever-changing times, the use of conventional energy resources is being questioned because of the effects they cause on the environment, and newer methods to produce or generate energy from natural resources are being taken into consideration. Such natural resources are termed renewable energy sources or RES. These RES mainly include wind, solar, hydro, and thermal resources. In this paper, a MATLAB/Simulink model for harnessing the energy from the wind with the help of a wind turbine is discussed. The design and simulation of this wind turbine will be discussed further in the paper and the rated power of this wind turbine is 6kW.

Keywords: Pitch Angle Control, Drive Train, Wind Turbine Matlab, Simulink, Simscape

# I. INTRODUCTION

The demand for wind energy generation has been increasing and is becoming a full industry with wind energy conversation systems (WECS). The basic science of WECS is simple, the wind is used to rotate the blades in a wind turbine, and the kinetic energy generated is converted into electricity by joining it to a generator. The energy generated either is sent through the grid or stored in a battery for personal use. In India, 37.5GW of the capacity of wind turbines are installed. It currently accounts for about 10% of India's total electricity capacity. The top five wind energy generation farms are situated at Muppandal Wind Farm (1500MW), Jaisalmer Wind Park (1064MW), Brahmanvel Wind Farm (528MW), Dhalgon Wind Farm (278MW), and Vankusawade Wind Park (259MW). A wind turbine can be VAWT and HAWT and in this paper, the design and simulation for a HAWT are discussed. A 6KW wind power generator is generally considered a small-scale wind turbine and in this paper, the design and simulation for it are going to be shown and discussed along with the various steps that were taken into consideration in order to achieve the desired output power.

#### **II. AIRFOIL**

An airfoil is the foundation of wind turbine blade design, it is the cross-section of a blade in a wind turbine, or a blade used in helicopters or a wing of an airplane and accordingly, we can change the design of the airfoil which can give us better performance and efficiency. An airfoil plays a major role in the input efficiency of the wind turbine. An arifoil with a suitable design in accordance with the setup used can help achieve a better input efficiency because then the swept area by the air will increase and the lift and drag forces acting on it will help rotate it much better thereby increasing the input efficiency of the mechanical input that is given to the generator via the rotatory shaft. The software that is used to design blades or the airfoil of the blade is Q-blade. This software provides various simulation and designing tools that hold predefined values and data about the various types of airfoil structures that have been used commercially to this date. It also has an inbuilt Cl/Cd or a Cp calculator that can be used to find out the lift and drag ratio of that specific blade or airfoil. The desired blade can also be designed by giving input parameters and a graphical representation can be obtained as well and from there, various blades and their airfoil design can be compared and the one which gives the best results can be selected. The airfoil here taken into consideration is the NACA 2414 and its properties are discussed below.



Fig -1: NACA 2414 Airfoil Design



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D FEM SPAST 🔨 🥆 360° - 🥠 Contraction of the second seco P K ▼ T1\_Re1.000\_M0.00\_N9.0 ▼
 -9.5 NACA 2414 NACA 2414-Re= 1000000-Alpha=-9 0.6 Polar Type = 1 Reynolds = 1 000 000 
 Reynolds = 1000 mpd
 000 000

 Mach = 0.000
 0.001

 Mach = 0.000
 0.015

 Forced Upper Trans. = 1.000
 1.000

 Alpha = -9.50 degr
 0.015

 Cd = -0.033
 Cm = -0.035

 Cd = 0.015
 0.015

 Upper Trans. = 0.028
 0.028
 Thickness = 14.00% Max. Thick.pos. = 29.50% Max. Camber = 2.00% Max. Camber pos. = 39.60% Number of Panels = 61 X = 0.622238, Y = -2.68138 Fig -2: Cp=Cl/Cd 1.5 1.0 0.5 Extra Points 1.6 1.0 0.8 0.6 0.4 1.0 0.8 0.6 0.4 0.2 Fig 3 -: Graphs of Cl, Cd and CP Circular Foil 0.060 m 0.160 m Circular Foil 0.260 m NACA-2414 0.360 m NACA 2414 0.460 m NAC 2414 0.560 m NAC 2414 0.660 m NAC 2414 0.760 m NACA 2414 0.860 m NACA-2414 0.960 m NACA 2414 1.060 m NACA 2414 Y

Fig -4: Obtained Airfoil by using the listed parameters



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# **III.ELECTRICAL COMPONENTS**

The proposed design is achieved using MATLAB and Simscape library in Simulink and running simulations have been carried out using Simulink. The various electrical components used in this design will be discussed further in the order in which they perform their functions in order to produce the desired range of electrical power. The components mainly have a wind turbine, two mass drive train, substations to get pitch angle, permanent magnet synchronous machine, three-phase V-I measurement, three-phase series RLC branch, voltage measurement, current measurement, RMS for voltage and current, first-order filter, two products, one divide, three gains of 1.732, -1, 1/152.8, three constants of 12 for wind speed, 8500, 152.8, eight scopes and two displays connected intricately as a network. In pitch angle substation includes one input for the energy wind turbine, one constant of one, one sum, one gain of 500, saturation, rate limiter, one scope, and one output of pitch angle. This circuitry consists of a reference input torque from the wind turbine or basically the variance in speed of the wind or rotation in blades which is positively summed to the gain of 500 which is element-wise gain (y = K.\*u). This is then connected to a saturation block which just limits the input signal to the upper and lower saturation values. This whole setup is then connected to a rate limiter which is limiting rising and falling rates of signal from -2 falling slew rate to 2 rising slew rate and finally, the pitch angle control is obtained. A scope is connected to obtain the graphical representation for the same. This PAC is a method of Maximum power point tracking employed in a wind turbine as PAC helps in always working towards getting the maximum power from the designed setup as MPPT algorithms are important in any renewable generation system. Wind energy system just like every other renewable energy generation system requires the to get as much energy as possible because according to Betz theory only 59.3% of total wind energy is converted into mechanical energy and hence wind turbine systems are operated at their maximum power point. Hence it is very crucial to have an MPPT procedure, PAC in this case to make the turbine operate at its maximum power point or optimal power point.



Fig -5: Pitch Angle Controller

$$\begin{split} \beta_{ref} &= \beta_0 = 0 \qquad for \ 0 < \Omega_t < \Omega_m \\ \beta_{ref} &= \frac{\Delta \beta}{\Delta \Omega} (\Omega_t - \Omega_m) + \beta_0 \qquad for \ \Omega_t > \Omega_m \\ \beta &= \frac{1}{(1 - t_\beta s)} \beta_{ref} \end{split}$$

🞦 Block Parameters: Gain						
Gain						
Element-wise gain ( $y = K.*u$ ) or matrix gain ( $y = K*u$ or $y = u*K$ ).						
Main	Signal Attributes Parameter Attributes					
Gain:	Gain:					
500						
Multiplication: Element-wise(K.*u)						





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Pa Block	Parameters: Sat	uration			$\times$
Saturat	ion				
Limit in	out signal to th	e upper and I	ower saturat	ion values.	
Main	Signal Attrib	ites			
Upper li	5				
45					:
Lower li	mit:				
0					:
✓ Treat	as gain when	linearizing			
	e zero-crossino				
		,			
0		ОК	Cancel	Help	Apply
		Fig -7: Satu	ration of PA	C	
Blog	k Parameters: Ra	•			$\times$
Rate L					
Limit r	sing and falling	g rates of sign	al.		
Param	eters				
Rising	slew rate:				
2					:
	slew rate:				
-2					:
	e time mode:	inherited			-
	condition:				
0					:
⊡ Tre	at as gain whe	n linearizing			
		ОК	Cancel	Help	Apply

#### Fig -8: Rate Limiter PAC







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A. Wind Turbine Function Block



Fig -10: Function block of Wind Turbine

Block Parameters: Wind Turbine   X							
Wind Turbine (mask) (link)							
This block implements a variable pitch wind turbine model. The performance coefficient Cp of the turbine is the mechanical output power of the turbine divided by wind power and a function of wind speed, rotational speed, and pitch angle (beta). Cp reaches its maximum value at zero beta. Select the wind-turbine power characteristics display to plot the turbine characteristics at the specified pitch angle.							
The first input is the generator speed in per unit of the generator base speed. For a synchronous or asynchronous generator, the base speed is the synchronous speed. For a permanent-magnet generator, the base speed is defined as the speed producing nominal voltage at no load. The second input is the blade pitch angle (beta) in degrees. The third input is the wind speed in m/s.							
The output is the torque applied to the generator shaft in per unit of the generator ratings.							
The turbine inertia must be added to the generator inertia.							
Parameters							
Nominal mechanical output power (W): 8.5e3							
Base power of the electrical generator (VA): 8.5e3/0.9							
Base wind speed (m/s): 12							
Maximum power at base wind speed (pu of nominal mechanical power): 0.8							
Base rotational speed (p.u. of base generator speed):							
Pitch angle beta to display wind-turbine power characteristics (beta >=0) (deg): 0							
Display wind turbine power characteristics							
OK Cancel Help Apply							

Fig -11: Block parameters of that Wind Turbine



B. Two Mass Drive Train Function Block



Fig -12: Function Block of 2 Mass Drive train



Fig -13: Design of the 2 Mass Drive train

In the above model, the torque input is given to the gain that is the wind turbine inertia constant which is then transferred to the wBase gain of the turbine which is then summed with mutual damping constant and the stiffness shaft spring constant, all of this along with the inverse gain is the shaft torque or that torque that is given to the generator as the mechanical input.

$$2Ht\frac{dwt}{dt} = Tm - Ts$$
(i)

$$\frac{1}{\text{webs}}\frac{d\theta \text{sta}}{dt} = \text{Wt} - \text{Wr}$$
(ii)



Fig -14: Torque Output characteristics



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## C. Modelling of a Permanent Magnet Synchronous Generator

The Permanent Magnet Synchronous Generator (PMSG) is used to produce electricity from the mechanical energy obtained from the wind. The two-phase synchronous reference frame is used to derive the dynamic model of the PMSG, which is the q-axis is 90° ahead of the d-axis with respect to the direction of rotation. In order to maintain synchronization between the two-phase quantity (d-q reference frame) and the three-phase quantity (abc three-phase frame) by using a phase-locked loop (PLL). The mathematical model of the PMSG in the synchronous reference frame (in the state equation form) is given by:

$$\frac{di_d}{dt} = \frac{1}{L_{ds} + L_{ls}} \left( -R_s I_d + \omega_e (L_{qs} + L_{ls}) i_q + u_d \right) (2)$$
$$\frac{di_q}{dt} = \frac{1}{L_{qs} + L_{ls}} \left( -R_s I_q - \omega_e [(L_{ds} + L_{ls}) i_d + \psi_f] + u_q \right) (3)$$

Here subscripts d and q refer to the physical quantities of rotating reference frame;  $R_s$  is the stator resistance,  $L_d$  and  $L_q$  are the d and q axis inductances of the generator,  $L_{ld}$  and  $L_{lq}$  are the d and q axis leakage inductances of the generator,  $\psi_f$  is the permanent magnetic flux and  $\omega_e$  is the electrical rotating speed of the generator. The electromagnetic torque equation of the PMSG is given by [4]

$$\tau_e = 1.5p\left((L_{ds} - L_{ls})i_d i_q + i_q \psi_f\right) \tag{4}$$

Where p is the number of pole pairs of the generator. The PMSG gives better performance compared to the induction generator because it does not have a rotor current. The additional advantage of using a PMSG is that you can use it without gearbox results in the reduction of cost and reduction of weight of the nacelle.



Fig -15: Block Function of PMSG

🞦 Block Parameters: Permanent Magnet Synchronous Machine	×							
Permanent Magnet Synchronous Machine (mask) (link)								
Implements a three-phase or a five-phase permanent magnet synchronous machine. The stator windings are connected in wye to an internal neutral point.								
The three-phase machine can have sinusoidal or trapezoidal back EMF waveform. The rotor can be round or salient-pole for the sinusoidal machine, it is round when the machine is trapezoidal. Preset models are available for the Sinusoidal back EMF machine.								
The five-phase machine has a sinusoidal back EMF waveform and round rotor.								
Configuration Parameters Advanced								
Machine parameters								
Compute from standard manufacturer specifications.								
Stator phase resistance Rs (Ohm): 0.425	:							
Armature inductance (H): 0.000395	:							
Machine constant	_							
Specify: Flux linkage established by magnets (V.s)								
Flux linkage: 0.433								
Inertia, viscous damping, pole pairs, static friction [ J(kg.m^2) F(N.m.s) p() Tf(N.m)]: 0.01197 0.001189 5 0]								
Initial conditions [ wm(rad/s) thetam(deg) ia,ib(A) ]: [0,0,0,0]	:							
Rotor flux position when theta = 0: Aligned with phase A axis (original Park)	•							
OK Cancel Help Apply								
Fig -16: Parameters of PMSG								



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🔁 Block Paramete	ers: Peri	manent Magne	et Syn <u>chronc</u>				×
Permanent Mag							
	nree-pl	hase or a five	e-phase pe	rmar		lagnet s	nchronous machine. The stator windings are
	the sin	usoidal mac	hine, it is r				k EMF waveform. The rotor can be round or hine is trapezoidal. Preset models are available
The five-phase r	machir	ne has a sinu	isoidal bac	k EMI	= wav	eform ar	d round rotor.
Configuration	Para	ameters A	Advanced				
Number of phase	es:	3					•
Back EMF wavef	orm:	Sinusoidal					
Rotor type:		Round					•
Mechanical input	t:	Torque Tm	1				
Preset model:		No					•
Measurement o	output						
			L- 51J	/: F	'aran	neters	of PMSG
Permanent Magnet Syn	nchronou		eter Calculator		aran	neters	of PMSG – 🗆
	nchronou	Specification	eter Calculator		'aran	neters	
ack EMF waveform	nchronou	Specification Sinusoidal	eter Calculator		aran	neters	- D Block Parameters
ack EMF waveform otor type		Specification Sinusoidal Round	eter Calculator		aran	neters	- 0
ck EMF waveform tor type sistance (ph-ph)	R	Specification Sinusoidal Round 0.36	eter Calculator		aran	neters	Block Parameters  Stator phase resistance Rs (ohm): 0 18  Armature inductance (H):
ack EMF waveform otor type esistance (ph-ph) ductance (ph-ph)	R Lab	Specification Sinusoidal Round 0.36 1.67	eter Calculator is V Ohm mH		aran	neters	Block Parameters  Stator phase resistance Rs (ohm): 0 18
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ck EMF waveform itor type sistance (ph-ph) ductance (ph-ph) axis inductance (ph) axis inductance (ph)	R Lab Ld Lq	Specification Sinusoidal Round 0.36 1.67 0	eter Calculator is V Ohm mH mH mH		aran	neters	Block Parameters  Stator phase resistance Rs (ohm): 0 18  Armature inductance (H):
tor type sistance (ph-ph) luctance (ph-ph) axis inductance (ph) axis inductance (ph)	R Lab Ld	Specification Sinusoidal Round 0.36 1.67	eter Calculator is V Ohm mH mH mH		aran	neters	Block Parameters  Stator phase resistance Rs (ohm):  0.18  Armature inductance (H):  0.000835  Flux linkage established by magnets (V.s):  0.0714394 Voltage Constant (Vpeak L-L / krpm):
ck EMF waveform tor type isistance (ph-ph) luctance (ph-ph) axis inductance (ph) axis inductance (ph) Sp	R Lab Ld Lq	Specification Sinusoidal Round 0.36 1.67 0	eter Calculator is V Ohm mH mH mH		/ kr		Block Parameters       Stator phase resistance Rs (ohm):       0.18       Armature inductance (H):       0.000835       Flux linkage established by magnets (V.s):       0.0714394       Voltage Constant (Vpeak L-L / krpm):       [518307
ack EMF waveform btor type esistance (ph-ph) ductance (ph-ph) axis inductance (ph) axis inductance (ph) Sp iltage constant	R Lab Ld Lq eecify:	Specification Sinusoidal Round 0.36 1.67 0 0 Torque const	eter Calculator is V Ohm mH mH tant V		/ kr;		Block Parameters  Stator phase resistance Rs (ohm):  0.18  Armature inductance (H):  0.000835  Flux linkage established by magnets (V.s):  0.0714394 Voltage Constant (Vpeak L-L / krpm):
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Permanent Magnet Syn ack EMF waveform otor type esistance (ph-ph) ductance (ph-ph) -axis inductance (ph) -axis inductance (ph) -axis inductance (ph) Sp oltage constant ertia scous damping ole pairs	R Lab Ld Lq Mecify: ke kt J F P	Specification           Sinusoidal           Round           0.36           1.67           0           0           0           0           60.70           5.5e-3           4.5           4	eter Calculator is V Ohm mH mH tant Vrms oz.in [b.in.s^2] oz.in/krpm meters	*	/ krr / Ар	m ▼) eak ▼)	Block Parameters       Block Parameters       Stator phase resistance Rs (ohm):       0.18       Armature inductance (H):       0.000835       Flux linkage established by magnets (V.5):       0.014394       Voltage Constant (Vpeak L-L / krpm):       51 8307       Torque Constant (N.m / Apeak):       0.428636       Inertia, friction factor, pole pairs [J(kg.m^2) F(N.m.s) p()]       [0.000621417 0.000303448 4]
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Fig -19: Voltage(V) Output



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Fig -20: Current(I) Output



Fig -21: SIMULINK Final Design of the proposed model for 6kW Wind Turbine





Fig -22: Generalised Graph of all the Outputs of the designed 6kW Wind Turbine



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J	601.7	
1		

Fig -23: 6kW output generated and observed from the display box of the SIMULINK

### **IV.CONCLUSIONS**

Wind energy is a better alternative to fossil fuels for the generation of electrical energy. It causes lesser pollution as compared to conventional resources and has a moderate maintenance cost as well. The simulation and design and the final results of the proposed 6kW were carried out successfully and the behavioural patterns were plotted graphically via the MATLAB/Simulink scope. Although, according to Betz theory only 59.3% of the total available 100% wind is converted into mechanical energy and hence windmills are operated at their maximum power point, and once such way to obtain that MPPT is by PAC which was also discussed and applied. This proposed design is believed to be more efficient than the trivial designs of a small 6kW wind turbine.

#### V. ACKNOWLEDGMENT

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